

AD-A091 717

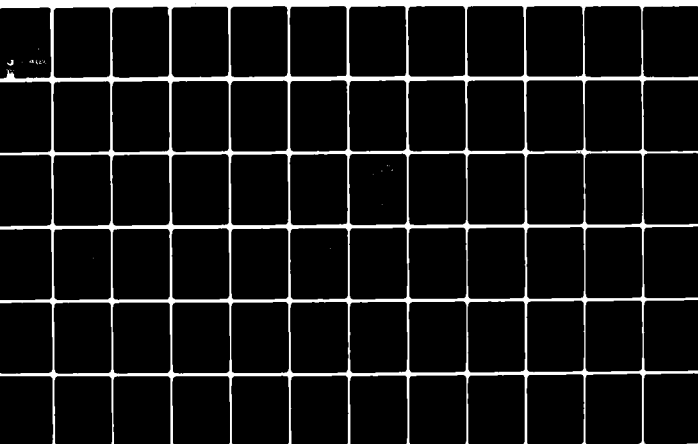
TENNESSEE UNIV KNOXVILLE DEPT OF CIVIL ENGINEERING F/G 4/2  
AIR FORCE RUNOFF MODEL (AFRUM) USER MANUAL DOCUMENTATION. (U)  
JUL 80 D E OVERTON, G W SCHLOSSNAGLE F08635-77-C-0254

UNCLASSIFIED

AFESC/ESL-TR-80-29

NL

1 OF 1  
ADA  
0917 7



END  
DATE  
FILMED  
12-80  
DTIC

AD A091717

LEVEL #

(2)

ESL-TR-80-29

# AIR FORCE RUNOFF MODEL (AFRUM) USER MANUAL DOCUMENTATION

D. E. OVERTON  
DEPARTMENT OF CIVIL ENGINEERING  
UNIVERSITY OF TENNESSEE  
KNOXVILLE, TENNESSEE 37916

G. W. SCHLOSSNAGLE, M. G. SIEBERT  
AIR FORCE ENGINEERING AND SERVICES CENTER

JULY 1980

FINAL REPORT

OCTOBER 1978 - JULY 1980

DTIC  
ELECTE  
NOV 20 1980  
S D  
A

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED



AFEGSC

ENGINEERING AND SERVICES LABORATORY  
AIR FORCE ENGINEERING AND SERVICES CENTER  
TYNDALL AIR FORCE BASE, FLORIDA 32403

8011 19 078

DC FILE COPY

NOTICE

Please do not request copies of this report from  
HQ AFESC/RD (Engineering and Services Laboratory).  
Additional copies may be purchased from:

National Technical Information Service  
5285 Port Royal Road  
Springfield, Virginia 22161

Federal Government agencies and their contractors  
registered with Defense Technical Information Center  
should direct requests for copies of this report to:

Defense Technical Information Center  
Cameron Station  
Alexandria, Virginia 22314

18 AFES/ESL

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

19 REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
1. REPORT NUMBER ESL-TR-86-29 ✓	2. GOVT ACCESSION NO. AD-A091 717	3. RECIPIENT'S CATALOG NUMBER	
4. TITLE (and Subtitle) AIR FORCE RUNOFF MODEL (AFRUM) USER MANUAL DOCUMENTATION •		5. TYPE OF REPORT & PERIOD COVERED Final Report • October 1978 — July 1980	
6. AUTHOR(s) Donald E. Overton George W. Schlossnagle Michael G. Siebert		7. PERFORMING ORG. REPORT NUMBER	
8. PERFORMING ORGANIZATION NAME AND ADDRESS Department of Civil Engineering University of Tennessee Knoxville, Tennessee 37916		9. CONTRACT OR GRANT NUMBER(s) F08635-77-C-0254 11	
10. CONTROLLING OFFICE NAME AND ADDRESS Air Force Engineering and Services Center Tyndall Air Force Base, Florida 32403		11. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS PF 62601F JON 1900-90-05 1790	
12. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) 12 81		13. REPORT DATE July 1980	
		14. NUMBER OF PAGES 74	
		15. SECURITY CLASS. (of this report) UNCLASSIFIED	
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.			
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)			
18. SUPPLEMENTARY NOTES Availability of this report is specified on verso of front cover.			
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Air Force Runoff Model      Airport Stormwater                      Simulation Runoff Computer Model			
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The Air Force Runoff Model (AFRUM) is a stormwater runoff simulation model designed to predict stormwater flow and quality resulting from real or design storms for small watersheds generally limited to 2,000 acres or less. The principal model inputs are watershed area, land use characteristics, percent forested, percent impervious, and percent denuded. The input will also include either an observed hydrograph or an estimated Soil Conservation Service Curve Number (CN). The model is based upon 410 storms in 36 watersheds. Output is both tabular and graphical and provides the watershed hydrograph, pollutograph,			

DD FORM 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

346680

11/10

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

20. ABSTRACT (Concluded).

- > and discussion of model assumptions. This report provides a background of the model, batch user instructions for CDC 6600 computers, and two example problems. The complete software package is provided in the Appendix.

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

## PREFACE

This report contains the Air Force Runoff Model (AFRUM) computer program user instructions and documentation developed during the period October 1978 - July 1980 under contract FO8635-77-C-0254 with the University of Tennessee, Knoxville, Tennessee 37916. Captain George W. Schlossnagle managed the project and modified the final product with the assistance of Sgt Mike Siebert to improve the user orientation.

A special thanks is given to the Grissom AFB civil engineers, civil engineering personnel and weather personnel, and the 6th Weather Squadron personnel of Tinker AFB for their excellent support of the project's data collection phase.

This report has been reviewed by the Public Affairs Office (PA) and is releasable to the National Technical Information Service (NTIS). At NTIS it will be available to the general public, including foreign nationals.

This technical report has been reviewed and is approved for publication.

GEORGE W. SCHLOSSNAGLE, Capt, USAF  
Water Quality Research Engineer

*Emil C. Frei*  
EMIL C. FREIN, LtCol, USAF  
Chief, Environics Division

MICHAEL G. MACNAUGHTON, LtCol, USAF, BSC  
Chief, Environics Division

*Robert E. Brandon*  
ROBERT E. BRANDON  
Dep Dir, Engrg & Services Lab.

1. Availability Codes  
 Avail and/or  
 Dist Special

## TABLE OF CONTENTS

Section	Title	Page
I.	Introduction.....	1
II.	Objective of AFRUM.....	3
III.	Hardware and Software Requirements.....	5
	1. Input Requirements.....	5
	2. Output Provided.....	7
IV.	Description of AFRUM.....	8
	1. Simulation of Direct Storm Runoff.....	8
	2. Simulation of Storm Hydrograph.....	10
	3. Simulation of Pollutant Yield.....	16
V.	Instructions for Data Preparation.....	19
VI.	Example Problems.....	24
	1. McDowell Ditch.....	24
	2. Capehart Marina.....	37
	References.....	51
Appendix		
A.	Listing of AFRUM.....	53

## LIST OF FIGURES

Figure	Title	Page
1	Double Triangle Model for Unit Response Function...	11
2	NURF for Various Land Use Conditions.....	14
3	Data Deck for AFRUM.....	20



# LIST OF TABLES

Table	Title	Page
1	Runoff Curve Numbers for Urban and Suburban Areas....	6
2	Coefficients in Pollutant Yield Model for Equation 12.....	18
3	AFRUM Card Data.....	21

## SECTION I

### INTRODUCTION

The Air Force Runoff Model (AFRUM) for simulating storm hydrographs and pollutant yields was developed for the U.S. Air Force by the Department of Civil Engineering at the University of Tennessee, Knoxville. The results of three separate but complementary studies had the same fundamental objectives, i.e., to evaluate the effects of specialized land use on stormwater runoff and its associated quality. The three studies were funded by the following three Federal agencies and dealt with the land use indicated:

<u>Federal Agency</u>	<u>Contract-Grant No.</u>	<u>Study</u>	
		<u>Period</u>	<u>Land Use</u>
U.S. Department of Energy	EY-76-S-05-4946	1975-79	Coal Strip Mining
U.S. Department of Interior Office of Water Resources Technology	TENN-A-046	1976-78	Urbanization
U.S. Air Force	F08635-77-C-0254	1975-79	Air Force Bases

AFRUM was developed in the course of analyzing 410 storms observed on 36 watersheds. The storm sample included watersheds

in agricultural, urban, and 100 percent forested land use conditions as well as watersheds undergoing coal strip mining and three watersheds at Grissom AFB, Indiana. AFRUM was extensively modified by the Air Force Engineering and Services Center, Tyndall Air Force Base, Florida to increase the user utility by modification of input and output formats and simplification of internal processes.

## SECTION II

### OBJECTIVE OF AFRUM

AFRUM was developed for the purpose of simulating stormwater hydrographs from a realtime or design storm rainfall distribution, land use and soil type of the watershed of interest. The watershed is considered to be a lumped system, and the required basin characteristics are percent of watershed that is forested (PF), percent that is impervious (PI), percent in strip mining or denuded (PS), and surface drainage area in square miles (SQMI).

Runoff volume and the associated rainfall excess time distribution are simulated from the input rainfall using the U.S. Soil Conservation Service Curve Number Model (Reference 1). If a runoff hydrograph (stormwater flow rates out of the basin) is read into the program associated with a rainfall hyetograph (rainfall distribution), the program will compute a Curve Number (CN) from this information. Otherwise, a CN must be read into the computer and would be simulated using the procedures specified in Reference 1.

AFRUM makes provision for simulating a unit hydrograph or unit response function (URF), which is convoluted with the rainfall excess hyetograph. This computer program is an adaptation of the simulation phase of the TVA double triangle model reported by Ardis (Reference 2) and later modified by Betson (Reference 3).

A more detailed description of the development of AFRUM has been reported by Overton, Troxler and Crosby (Reference 4), Overton and Crosby (Reference 5), and CEEDO-TR-77-18.

AFRUM also simulates pollutant loads for the associated storm. This simulation is a function of the specified watershed and storm characteristics. Hence, additional parameters are not needed.

## SECTION III

### HARDWARE AND SOFTWARE REQUIREMENTS

The computer model described in this manual is written in Fortran IV and operates on CDC 6600 computers under the NOSBE operating system. The program requires approximately 56K bytes of usable core capacity and approximately 6CPU seconds to compile and execute. Input is accomplished by a card reader, and the output is accomplished by a 132 position line printer. The plot subroutine, HYPLOT, within this program utilizes a Calcomp Electromechanical Plotter.

#### 1. Input Requirements

AFRUM accepts the following input:

a. Accumulated storm rainfall at equal time intervals, DT.

b. Stormwater discharge flow rates at equal time intervals, DT (this hydrograph may be used if available).

c. Watershed characteristics

(1) Curve Number (CN) which can be estimated using Table 1. If the hydrograph is read in, CN is calculated.

(2) Drainage area in square miles (SQMI).

(3) Percent forest (PF).

TABLE 1. RUNOFF CURVE NUMBERS FOR URBAN AND SUBURBAN AREAS  
(ANTECEDENT MOISTURE CONDITIONS II AND III;  $I_a = 0.2S$ )\*\*

		Curve numbers by antecedent moisture conditions							
		II				III			
Zoning Classification	Percent Imperviousness	Hydrologic Soil*				Hydrologic Soil*			
		A	B	C	D	A	B	C	D
Business, industrial, or commercial	75	82	88	90	91	92	95	96	97
Apartment houses	65	78	85	88	90	90	94	95	96
Schools	45	68	78	84	87	84	90	93	95
Urban residential (Lots $\pm$ 10,000 ft <sup>2</sup> )	40	65	77	83	86	82	89	93	94
Suburban residential (Lots $\pm$ 12,000 ft <sup>2</sup> )	35	62	76	82	85	80	89	92	94
Suburban residential (Lots $\pm$ 17,000 ft <sup>2</sup> )	30	60	74	81	84	78	88	92	93
Suburban residential	25	58	72	80	84	77	86	91	93
Parks and cemeteries	20	55	71	79	83	74	86	91	93
Unimproved areas	15	53	70	78	92	73	85	90	92
Lawns	0	45	65	75	80	66	82	88	91
Woods	0	36	60	73	79	-	-	-	-
Meadow (permanent)	0	30	58	71	78	-	-	-	-
Pasture or range	0	49	69	79	84	-	-	-	-

SCS National Engineering Handbook, Section 4, Table 15.1 "Percent of Imperviousness for Various Densities of Urban Occupancy."

\*Soils are divided into four hydrologic soils groups: A, B, C, and D. Group A soils have a high infiltration rate even when thoroughly wet. When thoroughly wet, group B soils have a moderate infiltration rate, group C soils have a slow infiltration rate, and group D soils have a very slow infiltration rate. Table 7.1 of Reference 1 lists more than 9,000 soils and their hydrologic group.

\*\*Antecedent Moisture Condition II is an average condition where III has the highest runoff potential. Condition II means soils in the watershed are practically saturated from antecedent rains.

- Data unavailable.

(4) Percent impervious (PI).

(5) Percent strip mined or denuded (PS).

2. Output provided

- a. Title banner page.
- b. Introduction to the model.
- c. Discussion of assumptions made by user.
- d. User input data.
- e. Adjusted model parameters.
- f. Simulated storm hydrograph (graphical and tabular).
- g. If read in, observed storm hydrograph (graphical and tabular).
- h. Suspended sediment storm load, Mn, Fe, Ca, Mg,  $\text{SO}_4$ , and total alkalinity storm loads.



## SECTION IV

### DESCRIPTION OF AFRUM

#### 1. Simulation of Direct Storm Runoff.

This program simulates direct runoff volume and rates using the Curve Number model of the U.S. Soil Conservation Service (Reference 1). All losses except evapotranspiration are lumped into a single initial abstraction. The model correlates the rainfall-direct runoff relations as a function of soil type, land use, and hydrologic condition.

For simple storms (high intensity and of short duration), the retention relative to the potential maximum retention  $S$  bears the following relation:

$$\frac{P - Q - I_a}{S} = \frac{Q}{P - I_a} \quad (1)$$

where  $P$  is storm rainfall in inches,  $Q$  is the direct storm runoff or effective rainfall in inches, and  $I_a$  is the initial abstraction in inches which is a measure of antecedent moisture. Initial abstraction includes surface storage, interception, and infiltration prior to runoff. The concept behind this method is for a given basin soil and land use condition, there is a maximum possible retention as storm rainfall increases, storm runoff will increase as defined by Equation (1). Storm runoff can be solved as follows:

$$Q = \frac{(P - I_a)^2}{(P - I_a) + S} \quad (2)$$

An empirical relation (Reference 6) for initial abstraction ( $I_a = 0.2S$ ) is inserted and Equation (2) becomes

$$Q = \frac{(P - 0.2S)^2}{P + 0.8S} \quad (3)$$

which is the relation used in the SCS method of estimating direct runoff from storm rainfall.

The runoff equation has been placed in graphical form with the main parameter being watershed retention,  $S$ , where  $S$  was related to the Curve Number,  $CN$ , as

$$S = \frac{1000}{CN} - 10 \quad (4)$$

Equations (2) and (4) show the interrelationships between  $CN$ , soils, land use, and hydrologic condition for average antecedent moisture conditions and are shown in the SCS Engineering Handbook (Reference 1) and summarized in Table 1.

Although Equation (3) was intended to simulate runoff volume it has been used extensively to simulate runoff rates by allowing  $P$  and  $Q$  in Equation (3) to represent accumulated storm rainfall and runoff volumes. Hence, incremental rainfall excess rates in each time period  $i_e(j)$  are simulated as

$$i_e(j) = \frac{Q(j) - Q(j-1)}{DT}$$

where  $Q(j)$  and  $Q(j-1)$  are accumulated storm runoff volume at times  $j \cdot DT$  and  $(j-1) \cdot DT$ , respectively, where  $j$  is the time increment number.

## 2. Simulation of Storm Hydrograph

### a. Normalized Unit Response Function (NURF)

The Unit Response Function (URF) in AFRUM is based upon Ardis' (Reference 2) quadrilateral function. The URF was coupled with the CN model to form the TVA double triangle model. The shape of the URFs and associated CNs have been optimized on a total of 410 storms in 36 watersheds.

The quadrilateral URF is based on the concept that the initial response from a watershed comes from the riparian areas, and as other areas of the watershed become saturated, they too begin to contribute to runoff in the form of a delayed response. It is assumed that these two responses can be simulated by two separate triangle response functions as shown in Figure 1. When added together, these two triangles form the quadrilateral unit response function.

Symbols used in the figure are:

$I$  = Precipitation excess intensity in inches per hour.  
Since the volume of input is one basin-inch =  $1/DT$ .

$DT$  = Time interval used in abstracting rainfall and discharge record in hours.

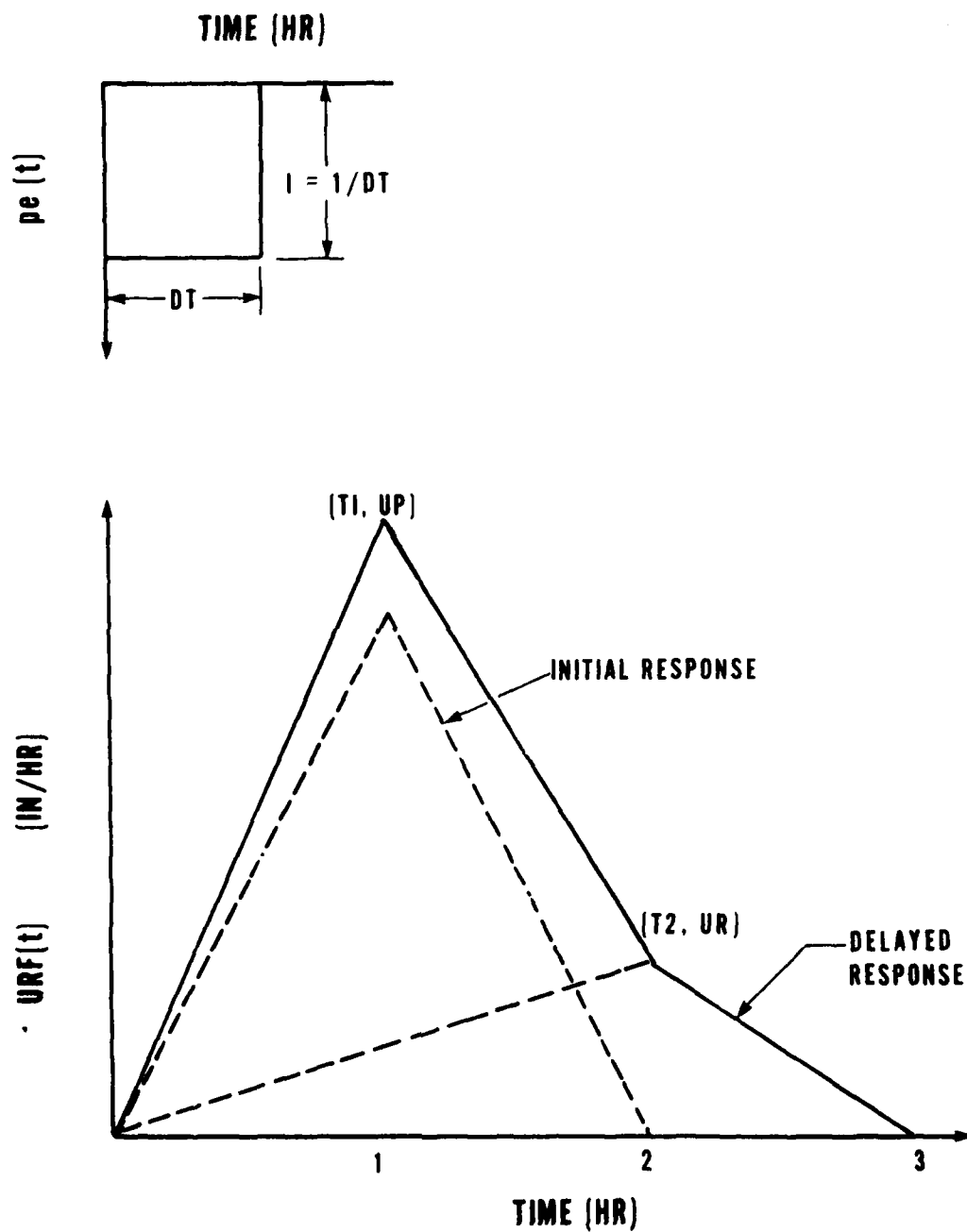


Figure 1. Double Triangle Model for Unit Response Function.

UP = Peak of unit response function at T1.

UR = Peak of delayed response at T2.

T1 = Time to peak of initial response, hours.

T2 = Time base of initial response and equal to the time of peak of delayed response, hours.

T3 = Time of end of delayed response, hours.

pe(t) = precipitation excess as a function of time, t, in inches per hour.

URF(t) = unit response function ordinate as a function of time, t, in inches per hour.

In deriving the URF, it is assumed that the peak of the delayed response (UR) occurs at the end of the initial response (T2), and the time bases of both responses and the time to peak of the initial response are integer multiples of DT. No assumption is made concerning the relative volumes contained in the initial and delayed responses or concerning the relative magnitudes of the peaks of the individual responses.

The double triangle URF is defined by the five parameters UP, UR, T1, T2, and T3. T3 is determined by:

$$T3 = (NOBS - NRAIN + 1) * DT$$

where NOBS = number of storm hydrograph ordinates in multiples of DT and NRAIN = number of rainfall increments in multiples of DT.

By maintaining a unit volume, UR is calculated from:

$$UR = (2 - [UP * T2] / [T3 - T1])$$

Therefore, defining a storm URF involves determining values of UP, T1, and T2.

The parameters UP, T1, and T2 are optimized using the pattern search technique. The objective function is the minimization of the sum of squares of errors between observed and simulated discharges. Since all five parameters describing the model are allowed to vary from storm to storm, the model is considered nonlinear. Rainfall excess is optimized using the SCS-Curve Number model after setting it equal to the observed direct runoff volume.

The variability of the URF from storm to storm within a watershed was explained by normalizing the time and discharge scale by the associated URF lag time, TL, where TL = time lapse between occurrences of 50 percent of the rainfall excess block and 50 percent of the URF volume. These normalized URFs are referred to as NURFs.

The NURF for each major land use category has been identified empirically, and are shown in Figure 2. The categories are: strip mined, 100 percent forest, urban without extensive storm sewers, urban with extensive storm sewers, and agricultural. As a matter of providing a reference, the NURF

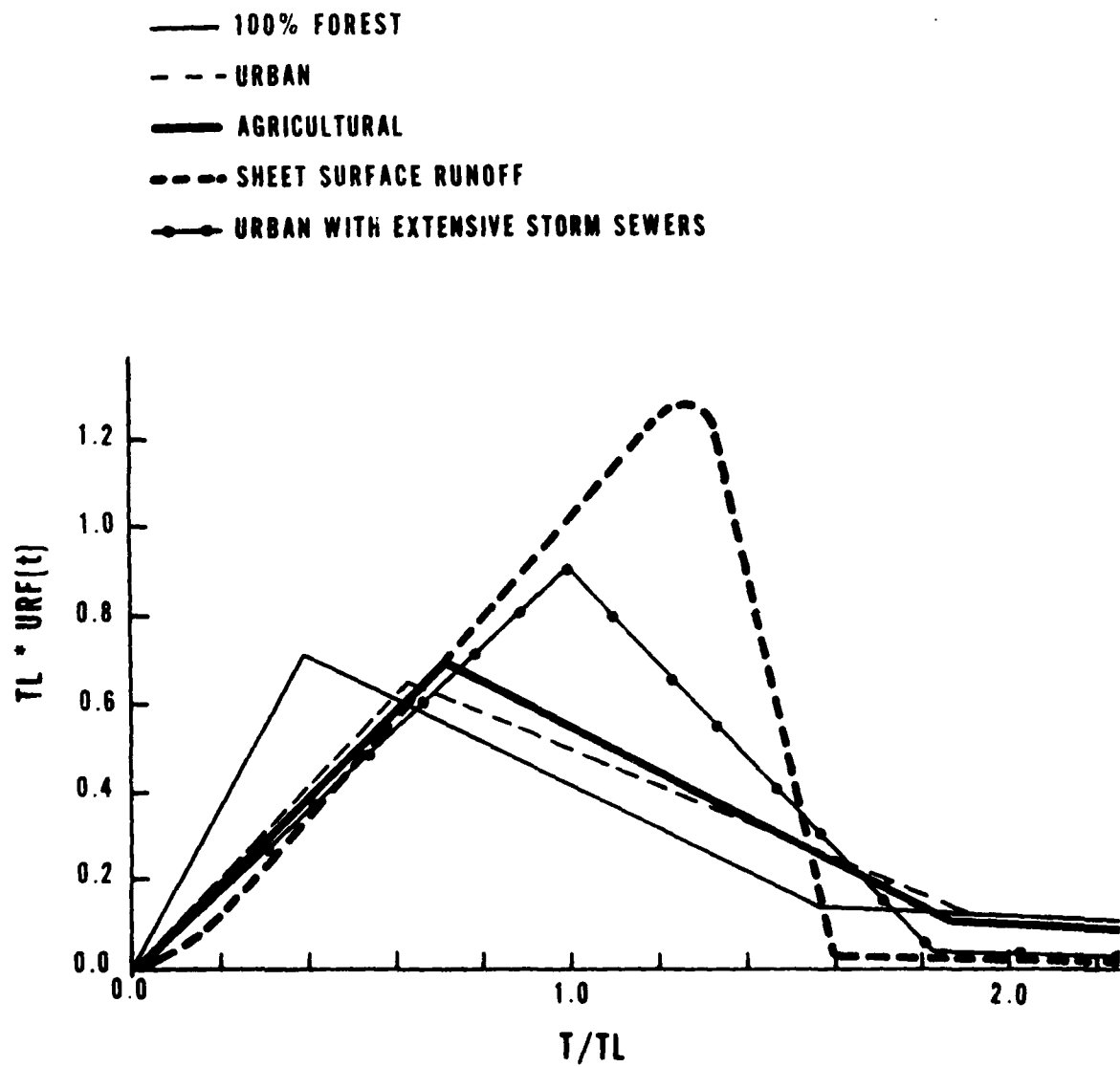


Figure 2. NURF for Various Land Use Conditions.

observed for sheet surface runoff from a plane (Reference 6) is shown. The strip mined watersheds were previously in 100 percent forested areas. Hence, a pattern is shown where the forested and strip mined watersheds have a small initial response whereas the urban and agricultural watersheds have a larger initial response. This implies that imperviousness and crop land produce much more surface runoff. The storm sewered NURF has an even higher initial response, which is generated by runoff collection systems. Sheet surface runoff has no delayed response.

b. Lag Time

Lag time, TL, for a storm is simulated in AFRUM using the concept that it varies inversely with the rainfall excess intensity. AFRUM uses a weighted rainfall excess intensity (WRE)

$$WRE = \frac{\sum_{j=1}^N i_e^2(j)}{\sum_{j=1}^N i_e(j)} \quad (8)$$

where N is the number of time intervals equal to DT. The weighted storm rainfall intensity is given the exponent 0.4 (References 4 and 5). The following equation is used to calculate the time lag

$$TL \text{ (min)} = \mu / WRE^{0.4} \quad (9)$$

where lag modulus,  $\mu$ , is empirically related to watershed characteristics in the following manner:



(1) For rural watersheds

$$\mu(\text{hr}) = 0.060 * \text{SQMI} + 0.0203 * \text{PF} + 1.16 \quad (10)$$

(2) For urban watersheds

$$\mu(\text{hr}) = 3.24 (\text{SQMI}/\text{PI})^{0.6} \quad (11)$$

c. Convolution of URF

The final step in simulating a stormwater hydrograph is to convolute the storm URF with the rainfall excess time distribution. The URF is defined by simulating storm lag time from Equation (9) using with either Equation (10) or (11), depending on the watershed land use. WRE is calculated by Equation (8).

3. Simulation of Pollutant Yield

a. Load Modulus

AFRUM simulates storm pollutant yield using a load modulus (lb/acre-in of storm runoff) as a function of percent stripped or denuded (PS), lag modulus ( $\mu$ ), and percent forest or trees (PF), in the following form:

$$\mu_w = C_1 * \text{PS} - C_2 * \mu * \text{PF} + C_3 \quad (12)$$

The coefficients were optimized using stormwater quality data on a total of eleven watersheds; six of them were undergoing coal

strip mining and five were urbanized (Reference 5). Equation (12) was derived from a mass balance, and each of its terms represents a component of pollutant yield.

$C_1 * PS$  = source of pollutant or soil loss

$C_2 * \mu * PF$  = deposition between source and outfall, and

$C_3$  = storage in watershed picked up and redeposited.

The coefficients optimized for the coal strip mined and urbanized watersheds are shown in Table 2. The coefficients were previously presented in References 4 and 5.

b. Storm Load

Once load modulus for the watershed pollutant has been simulated, the storm pollutant yield, SPY, is simulated by

$$SPY = \mu_w * AREA * 640 * SRO \quad (13)$$

where SRO is the total storm runoff in surface inches, and AREA is in acres.

TABLE 2. COEFFICIENTS IN POLLUTANT YIELD MODEL

FOR EQUATION (12)

## URBAN

Pollutant	Coefficients		
	Source $C_1$	Deposition $C_2$	Storage $C_3$
Suspended Solids	16.7	21.5	62.3
Fe	0.442	0.568	1.54
Mn	0.0072	0.0092	0.20
Ca	0.147	0.189	2.45
Mg	0.0597	0.113	0.0323
Sulfate	0.0719	0.0216	1.24
Total Alkalinity	0.319	0.128	6.71

## COAL STRIP MINED (Active)

Suspended Solids	18.2	1.28	576.7
Fe	0.323	0	0.12
Mn	0.0161	0	0.002
Ca	0.131	0	0.38
Mg	0.133	0	0.40
Sulfate	1.39	0	2.45
Total Alkalinity	0.19	0	2.00

## SECTION V

### INSTRUCTIONS FOR DATA PREPARATION

The data cards should be prepared according to Figure 3 and Table 3. Figure 3 shows the layout of the data cards in the order in which they must be read into the computer. Table 3 shows how the data are to be punched and lists the description of variables used in the program.

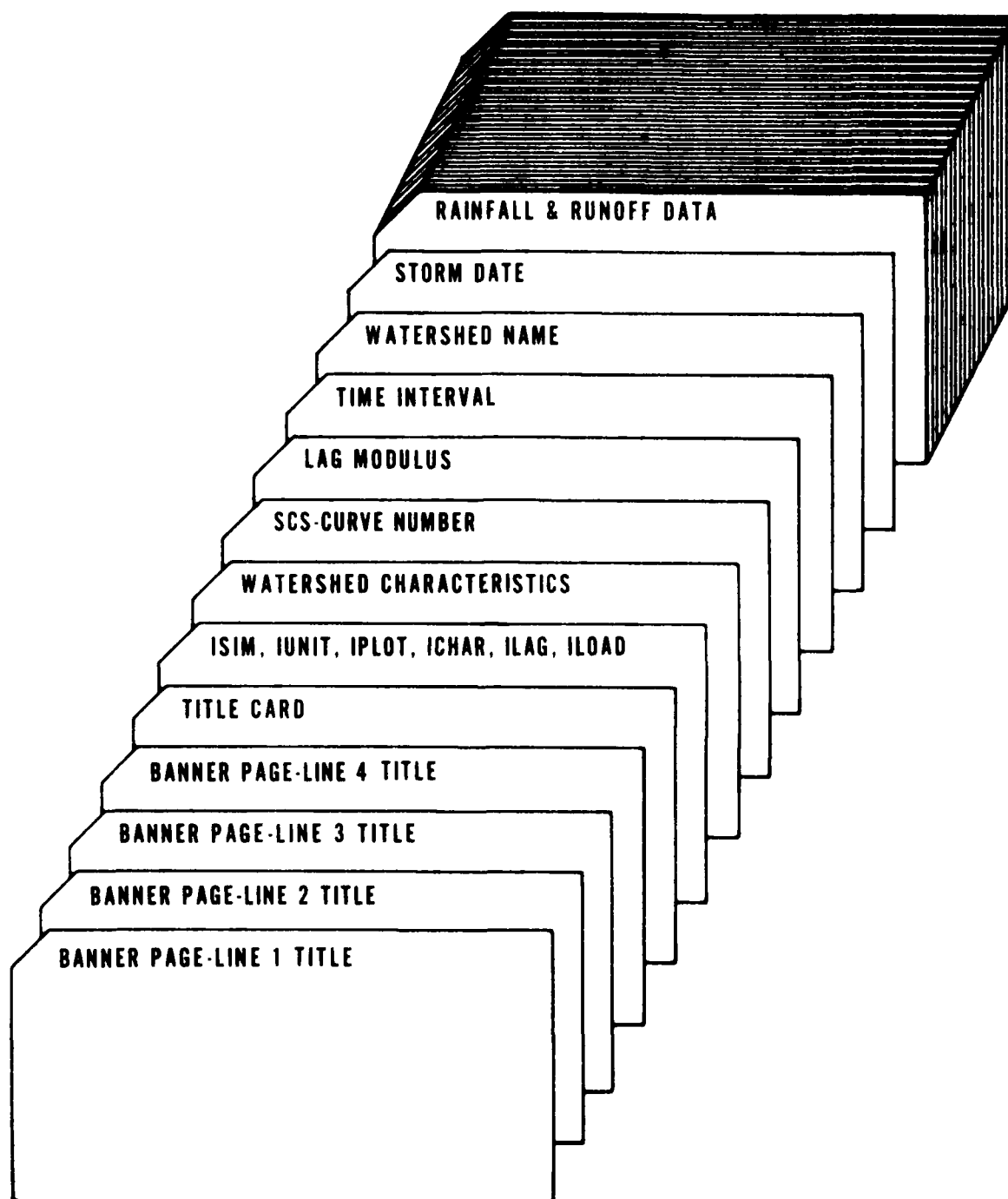


Figure 3. Data Deck for AFRUM

TABLE 3. AFRUM CARD DATA

## U.S. AIR FORCE RUNOFF MODEL (AFRUM)

A STORM HYDROGRAPH SIMULATION MODEL DEVELOPED FOR THE AIR FORCE ENGINEERING SERVICES CENTER, TYNDALL AFB, FLORIDA BY DR DONALD OVERTON OF THE UNIVERSITY OF TENNESSEE, PRINCIPAL INVESTIGATOR AND GEORGE W. SCHLOSSNAGLE, CAPT USAF, BSC, PROJECT OFFICER

AFRUM		
CARD NO.	FORMAT/ COLUMNS	VARIABLE NAMES AND DESCRIPTION
1	(12A1)/ (1-12)	BANNER PAGE - 1ST LINE -- USER DESCRIPTION
2	(12A1)/ (1-12)	BANNER PAGE - 2ND LINE -- USER DESCRIPTION
3	(12A1)/ (1-12)	BANNER PAGE - 3RD LINE -- USER DESCRIPTION
4	(12A1)/ (1-12)	BANNER PAGE - 4TH LINE -- USER DESCRIPTION
5	(20A4)/ (1-80)	TITLE NAME AND LOCATION OF WATERSHED
6	(6I4)/ (1-4)	ISIM,IUNIT,IPL0T,ICHAR,ILAG,ILOAD ISIM-A CONTROL VARIABLE TO SPECIFY THE TYPE OF DATA SUPPLIED TO THE PROGRAM ISIM=1 ONLY RAINFALL DATA IS SUPPLIED AND AN ESTIMATE MUST BE MADE OF THE SCS CURVE NUMBER
	(5-8)	IUNIT-A CONTROL PARAMETER TO SPECIFY OUTPUT UNITS OF SIMULATED HYDROGRAPH IUNIT=0 UNITS ARE IN INCHES/HR IUNIT=1 UNITS ARE IN CFS
	(9-12)	IPL0T-A CONTROL PARAMETER TO DETERMINE IF OUTPUT IS PLOTTED IPL0T=0 NO PLOT IS PRODUCED IPL0T=1 A PLOT IS PRODUCED
	(13-16)	ICHAR-A CONTROL PARAMETER TO SPECIFY IF LAND USE IS URBAN (WITH OR WITHOUT EXTENSIVE STORM SEWERS), AGRICULTURAL, COAL STRIP MINED OR 100% FOREST ICHAR=0 URBAN WITHOUT STORM SEWERS ICHAR=1 URBAN WITH STORM SEWERS ICHAR=2 COAL STRIP MINED ICHAR=3 AGRICULTURAL ICHAR=4 FORESTED

TABLE 3. AFRUM CARD DATA (CONTINUED)

(17-20) ILAG-A CONTROL PARAMETER TO DETERMINE IF LAG  
MODULUS IS READ IN OR SIMULATED FROM  
WATERSHED CHARACTERISTICS  
ILAG=0 LAG MODULUS IS READ IN  
ILAG=1 LAG MODULUS IS SIMULATED FROM URBAN  
WATERSHED CHARACTERISTICS (% IMPERVIOUS  
AND AREA [SQMI])  
ILAG=2 LAG MODULUS IS SIMULATED FROM RURAL  
WATERSHED CHARACTERISTICS (% FOREST AND  
AREA [SQMI])  
(21-24) ILOAD-A CONTROL PARAMETER TO DETERMINE HOW  
SUSPENDED SEDIMENT STORM LOAD IS TO BE  
SIMULATED FROM % FOREST, % IMPERVIOUS,  
% STRIPPED AND LAG MODULUS  
ILOAD=1 URBAN WATERSHED  
ILOAD=2 COAL STRIP MINED WATERSHED

WATERSHED CHARACTERISTICS: ID URBAN,PS=0; IF RURAL,PI=0  
7 (4F8.0)/ SQMI,PF,PS,PI

(1-8) SQMI=WATERSHED AREA IN SQUARE MILES  
(9-16) PF=PERCENT FOREST  
(17-24) PS=PERCENT COAL STRIP MINED (OR DENUDED)

CARD A IS NOT REQUIRED IF ISIM=0 (CARD 5)

8 (F10.0)/ CN  
(1-10) CN=SCS CURVE NUMBER FOR WATERSHED AT THE TIME  
THE STORM OCCURED (VARIES WITH ANTECEDENT  
MOISTURE)

CARD 9 IS NOT REQUIRED IF ILAG=1 or 2 (CARD 5)

9 (F10.0)/ U  
(1-10) U=LAG MODULUS, HOURS  
10 (F10.0)/ DT  
(1-10)1 DT=TIME INTERVAL USED IN ABSTRACTING RAINFALL  
(HRS)

CARD 11,12, and 13 MUST BE REPEATED FOR EACH STORM TO BE  
SIMULATED

11 (8A4)/ BASIN  
(1-32) BASIN=NAME OF WATERSHED

TABLE 3. AFRUM CARD DATA (CONCLUDED)

12	(2A4)/	BDATE BDATE=DATE OF STORM
13	(I1,9X, F10.3,30X, F10.3)/ (1)	ISTAGE,RAIN(I),SFLOW(I)
		ISTAGE-A CONTROL PARAMETER TO SIGNAL THE END OF A STORM DATA SET
		ISTAGE=0 SIGNALS CONTINUATION OF RAINFALL/ RUNOFF
		ISTAGE=1 SIGNALS LAST DATA CARD OF A STORM
	(2-10)	BLANK
	(11-20)	RAIN(I) RAIN(I)=CUMULATIVE STORM RAINFALL ABSTRACTED AT DT TIME INTERVALS. THE FIRST VALUE OF RAIN(I) MUST BE 0.0 AT TIME 0.0
	(21-50)	BLANK
	(51-60)	SFLOW(I) SFLOW(I)=STORMWATER DISCHARGED IN CFS, ABSTRACTED AT DT TIME INTERVALS, VALUES OF SFLOW(I) ARE NOT REQUIRED IF ISIM=1 (CARD 1). THE FIRST AND LAST VALUES OF SFLOW(I) MUST BE 0.0

NO. OF RAINFALL/RUNOFF CARDS MUST BE EQUAL TO NUMBER OF RAINFALL/  
RUNOFF OBSERVATIONS  
A MAXIMUM OF 500 RAINFALL/RUNOFF OBSERVATIONS MAY BE SUBMITTED



## SECTION VI

### EXAMPLE PROBLEMS

#### 1. McDowell Ditch

An example application of AFRUM is provided for the McDowell Ditch watershed at Grissom Air Force Base, Indiana. The watershed is 276 acres in size, has 20 percent imperviousness, and essentially zero percent trees. The soils are classified in SCS group C and watershed land use is considered to be urban without extensive storm sewers.

The accumulated rainfall and hydrograph for the storm of November 14, 1978 was measured for the McDowell watershed. Since the runoff was available, the storm CN was calculated within AFRUM. However, using the SCS-CN method (see Table 3) the CN for the storm was estimated to be 83, whereas the calculated CN using storm rainfall and runoff was 81. This produced an error of 3.1 percent.

Hence, the data was punched onto the cards into the specified format and entered into the computer after the appropriate JCLs. A listing of the input and the program output follows.



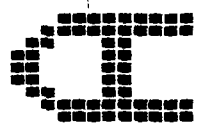






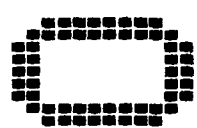
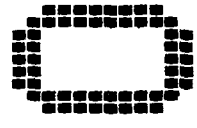















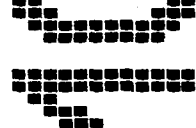

AFRUM  
 GRISSOM AFH  
 14 NOV 78  
 MCDOWELL DIT

0 1 1 0 1 1  
 0.43 5.5 0.0 22.0  
 0.25  
 MCDOWELL DITCH  
 11-14-78

0.0  
 0.05  
 0.10  
 0.15  
 0.20  
 0.20  
 0.20  
 0.20  
 0.20  
 0.30  
 0.31  
 0.34  
 0.35  
 0.40  
 0.43  
 0.48  
 0.55  
 0.60  
 0.70  
 0.82  
 0.92  
 1.00  
 1.08  
 1.14  
 1.21  
 1.23  
 1.24  
 1.26  
 1.27  
 1.28  
 1.29  
 1.30  
 1.30  
 1.33  
 1.36  
 1.38  
 1.38  
 1.45  
 1.46  
 1.47  
 1.47  
 1.47  
 1.48  
 1.48  
 1.49

0.006  
 0.2  
 0.3  
 0.6  
 1.1  
 1.7  
 2.5  
 3.5  
 4.6  
 5.8  
 6.5  
 7.6  
 8.5  
 9.7  
 10.8  
 11.6  
 12.1  
 12.6  
 13.0  
 12.4  
 11.6  
 10.7  
 9.9  
 8.9  
 7.9  
 7.7  
 7.5  
 7.7  
 7.9  
 7.7  
 7.5  
 7.3  
 7.1  
 7.0  
 6.7  
 6.6  
 6.4  
 6.2  
 5.0



## INTRODUCTION

THE U.S. AIR FORCE RUNOFF MODEL (AFRUM) FOR SIMULATING STORM HYDROGRAPHS AND POLLUTANT YIELDS WAS DEVELOPED FOR THE AIR FORCE BY THE DEPARTMENT OF CIVIL ENGINEERING, UNIVERSITY OF TENNESSEE, KNOXVILLE AND THE RESEARCH AND DEVELOPMENT DIRECTORATE OF THE AIR FORCE ENGINEERING SERVICES CENTER (AFESC), TYNDALL AIR FORCE BASE, FLORIDA. DR. DONALD E. OVERTON OF THE UNIVERSITY OF TENNESSEE WAS THE PRINCIPAL INVESTIGATOR AND DR. GEORGE W. SCHLOSSNAGLE OF THE U.S. AIR FORCE WAS THE PROJECT OFFICER. THE RESULTS OF THREE SEPARATE BUT COMPLEMENTARY STUDIES WERE INCORPORATED INTO AFRUM. EACH OF THE THREE STUDIES HAD THE FUNDAMENTAL OBJECTIVE TO EVALUATE THE EFFECTS OF SPECIALIZED LAND USE ON STORMWATER RUNOFF AND ITS ASSOCIATED QUALITY. THE THREE STUDIES WERE FUNDED BY THE U.S. DEPARTMENT OF ENERGY, THE U.S. DEPARTMENT OF INTERIOR AND THE U.S. AIR FORCE. THE STUDY PERIOD WAS FROM 1975 THROUGH 1979. AFRUM WAS DEVELOPED IN THE COURSE OF ANALYZING 410 STORM EVENTS ON 36 WATERSHEDS, WHICH INCLUDED AGRICULTURAL, URBAN AND FORESTED LAND USE CONDITIONS AS WELL AS COAL STRIP MINING AND THREE WATERSHEDS ON A U.S. AIR FORCE BASE.

AFRUM WAS DEVELOPED FOR THE PURPOSE OF SIMULATING STORMWATER HYDROGRAPHS FROM ACTUAL OR DESIGN STORM RAINFALL DISTRIBUTIONS, LAND USE CHARACTERISTICS AND SOIL TYPE IN THE WATERSHED OF CONCERN. THE REQUIRED INPUT BASIN CHARACTERISTICS ARE:

1. PERCENT OF WATERSHED THAT IS FORESTED
2. PERCENT OF WATERSHED THAT IS IMPERVIOUS
3. PERCENT OF WATERSHED THAT IS DENUDED OR STRIP MINED
4. SURFACE DRAINAGE AREA

RUNOFF VOLUME AND THE ASSOCIATED RAINFALL EXCESS TIME DISTRIBUTION ARE SIMULATED FROM INPUT RAINFALL USING THE U.S. SOIL CONSERVATION SERVICE CURVE NUMBER. IF A RUNOFF HYDROGRAPH IS PROVIDED WITH THE ASSOCIATED RAINFALL HYETOGRAPH, AFRUM WILL COMPUTE THE CURVE NUMBER, CN; OTHERWISE CN MUST BE AN INPUT. CN IS SELECTED BY USING THE PROCEDURES PROVIDED IN THE NATIONAL ENGINEERING HANDBOOK, SECTION 4, U.S. SOIL CONSERVATION SERVICE.

AFRUM MAKES PROVISION FOR SIMULATING A UNIT HYDROGRAPH OR UNIT RESPONSE FUNCTION, WHICH IS CONVOLUTED WITH THE RAINFALL EXCESS HYETOGRAPH. AFRUM ALSO SIMULATES POLLUTANT LOADS FOR THE INPUTED STORM. THIS SIMULATION IS A FUNCTION OF THE SPECIFIED WATERSHED AND STORM CHARACTERISTICS.

GRISSOM AFB

THE WATERSHED NAME IS MCDOWELL DITCH  
THE DATE OF THE RAINFALL EVENT IS 11-14-78  
THE WATERSHED SIZE IN SQUARE MILES IS: SQMI= .43  
THE PERCENT OF THE BASIN WHICH IS FOREST IS: PF= 5.50  
THE PERCENT OF THE BASIN DENUDED IS: PS= 0.00  
THE PERCENT OF THE BASIN WHICH IS IMPERVIOUS IS: PI= 22.00

BY SETTING ISIM = 0 YOU HAVE INDICATED THAT YOU PLAN  
TO SUPPLY EITHER ACTUAL OR DESIGN RAINFALL AND RUNOFF  
DATA; THEREFORE, THE SCS CURVE NUMBER, CN, WILL BE DE-  
TERMINED BY SETTING RUNOFF EQUAL TO PRECIPITATION EXCESS.

OUTPUT UNITS OF THE SIMULATED HYDROGRAPH ARE HOURS  
AND CUBIC FEET PER SECOND, CFS, AS SELECTED BY SETTING  
IUNIT = 1.

YOU HAVE REQUESTED THAT THE HYDROGRAPH BE PLOTTED  
BY SETTING IPLOT = 1.

THE WATERSHED IS ASSUMED TO BE URBAN WITHOUT  
STORM SEWERS; ICHAR = 0.

YOU HAVE ELECTED TO SIMULATE LAG MODULUS IN  
HOURS ASSUMING IT IS A FUNCTION OF THE WATERSHED AREA  
AND PERCENT IMPERVIOUS AREA OF THE WATERSHED; ILAG = 1.

SEDIMENT LOAD HAS BEEN SIMULATED ASSUMING THE  
WATERSHED IS RURAL OR URBAN WITHOUT MAJOR CONSTRUCTION;  
ILOAD = 1.

TABLE I. USER INPUT

TIME (HR)	TOTAL RAIN (IN)	INCREMENTAL RAIN (IN)	OBSERVED FLOW (CFS)	DATA FLOW (IN/HR)
0.00	0.00	0.00	0.00	0.000000
.25	.05	.05	0.00	0.000000
.50	.10	.05	0.00	0.000000
.75	.15	.05	0.00	0.000000
1.00	.20	.05	0.00	0.000000
1.25	.200	0.000	0.00	0.000000
1.50	.200	0.000	0.00	0.000000
1.75	.200	0.000	0.00	0.000000
2.00	.200	0.000	0.00	0.000000
2.25	.30	.10	0.00	0.000000
2.50	.31	.01	0.00	0.000000
2.75	.34	.03	0.00	0.000000
3.00	.35	.01	0.00	0.000000
3.25	.40	.05	0.00	0.000000
3.50	.43	.03	0.00	0.000000
3.75	.48	.05	0.00	0.000000
4.00	.55	.07	0.00	0.000000
4.25	.60	.05	0.00	0.000000
4.50	.70	.10	0.00	0.000000
4.75	.82	.12	0.00	0.000000
5.00	.92	.10	0.00	0.000000
5.25	1.000	.08	0.00	0.000000
5.50	1.08	.08	0.00	0.000000
5.75	1.14	.06	0.00	0.000000
6.00	1.21	.07	0.00	0.000000
6.25	1.23	.02	.01	.000002
6.50	1.26	.01	.20	.000072
6.75	1.27	.02	.30	.00108
7.00	1.27	.01	.60	.00216
7.25	1.28	.01	1.10	.00396
7.50	1.29	.01	1.70	.00613
7.75	1.30	.01	2.50	.00901
8.00	1.30	0.00	3.50	.01261
8.25	1.33	.03	4.60	.01658
8.50	1.36	.03	5.80	.02090
8.75	1.38	.02	6.50	.02342
9.00	1.38	0.00	7.60	.02739
9.25	1.45	.07	8.50	.03063
9.50	1.46	.01	9.70	.03496
9.75	1.47	.01	10.80	.03892
10.00	1.47	0.00	11.60	.04180
10.25	1.47	0.00	12.10	.04360
10.50	1.48	.01	12.60	.04541
10.75	1.48	0.00	13.00	.04685
11.00	1.49	.01	12.40	.04469
11.25	0.00	0.00	11.60	.04180
11.50	0.00	0.00	10.70	.03856
11.75	0.00	0.00	9.90	.03568
12.00	0.00	0.00	8.90	.03207
12.25	0.00	0.00	7.90	.02847
12.50	0.00	0.00	7.70	.02775
12.75	0.00	0.00	7.50	.02703
13.00	0.00	0.00	7.70	.02775
13.25	0.00	0.00	7.90	.02847
13.50	0.00	0.00	7.70	.02775
13.75	0.00	0.00	7.50	.02703
14.00	0.00	0.00	7.30	.02631
14.25	0.00	0.00	7.10	.02559
14.50	0.00	0.00	7.00	.02523
14.75	0.00	0.00	6.70	.02414
15.00	0.00	0.00	6.60	.02378
15.25	0.00	0.00	6.40	.02306
15.50	0.00	0.00	6.20	.02234
15.75	0.00	0.00	5.00	.01802

TABLE I. USER INPUT (CONTINUED)

16.00	0.00	0.00	4.70	.01694
16.25	0.00	0.00	4.40	.01586
16.50	0.00	0.00	4.20	.01514
16.75	0.00	0.00	4.10	.01478
17.00	0.00	0.00	3.80	.01369
17.25	0.00	0.00	3.50	.01261
17.50	0.00	0.00	3.20	.01153
17.75	0.00	0.00	2.90	.01045
18.00	0.00	0.00	2.90	.01045
18.25	0.00	0.00	2.90	.01045
18.50	0.00	0.00	2.90	.01045
18.75	0.00	0.00	2.90	.01045
19.00	0.00	0.00	2.90	.01045
19.25	0.00	0.00	2.40	.00865
19.50	0.00	0.00	2.10	.00757
19.75	0.00	0.00	1.90	.00685
20.00	0.00	0.00	1.80	.00649
20.25	0.00	0.00	1.80	.00649
20.50	0.00	0.00	1.60	.00577
20.75	0.00	0.00	1.50	.00541
21.00	0.00	0.00	1.40	.00505
21.25	0.00	0.00	1.30	.00468
21.50	0.00	0.00	1.20	.00432
21.75	0.00	0.00	1.10	.00396
22.00	0.00	0.00	1.00	.00360
22.25	0.00	0.00	.90	.00324
22.50	0.00	0.00	.80	.00288
22.75	0.00	0.00	.80	.00288
23.00	0.00	0.00	.80	.00288
23.25	0.00	0.00	.80	.00288
23.50	0.00	0.00	.80	.00288
23.75	0.00	0.00	.75	.00270
24.00	0.00	0.00	.71	.00256
24.25	0.00	0.00	.65	.00234
24.50	0.00	0.00	.61	.00220
24.75	0.00	0.00	.61	.00220
25.00	0.00	0.00	.60	.00216
25.25	0.00	0.00	.60	.00216
25.50	0.00	0.00	.55	.00198
25.75	0.00	0.00	.47	.00169
26.00	0.00	0.00	.47	.00169
26.25	0.00	0.00	.47	.00169
26.50	0.00	0.00	.47	.00169
26.75	0.00	0.00	.47	.00169
27.00	0.00	0.00	.47	.00169
27.25	0.00	0.00	.47	.00169
27.50	0.00	0.00	.47	.00169
27.75	0.00	0.00	.43	.00155
28.00	0.00	0.00	.40	.00144
28.25	0.00	0.00	.37	.00133
28.50	0.00	0.00	.33	.00119
28.75	0.00	0.00	.32	.00115
29.00	0.00	0.00	.30	.00108
29.25	0.00	0.00	.29	.00105
29.50	0.00	0.00	.28	.00101
29.75	0.00	0.00	.28	.00101
30.00	0.00	0.00	.27	.00097
30.25	0.00	0.00	.26	.00094
30.50	0.00	0.00	.24	.00086
30.75	0.00	0.00	.24	.00086
31.00	0.00	0.00	.24	.00086
31.25	0.00	0.00	.24	.00086
31.50	0.00	0.00	.24	.00086
31.75	0.00	0.00	.23	.00083
32.00	0.00	0.00	.23	.00083
32.25	0.00	0.00	.22	.00079



TABLE I. USER INPUT (CONCLUDED)

32.75	0.00	0.00	.22	.00079					
33.00	0.00	0.00	.10	.00036					
33.25	0.00	0.00	.05	.00018					
33.50	0.00	0.00	0.00	0.00000					
ADJUSTED HYDROGRAPH PARAMETERS									
RFI .085	U .306	N .400	TL .820	UP .809	UR .146	T1 .500	T2 1.500	T3 5.750	AREA .991
UP .816	UR .148	T1 .500	T2 1.500	T3 5.750	AREA 1.000				

TABLE II. HYDROGRAPH OUTPUT

OBSERVED FLOW OUT OF WATERSHED (CFS)	PREDICTED FLOW OUT OF WATERSHED (CFS)	TIME (HOURS)	SUSPENDED SOLIDS DISCHARGED FROM WATERSHED LBS/SEC
0.000	0.000	0.000	0.000
0.000	0.000	.250	0.000
0.000	0.000	.500	0.000
0.000	0.000	.750	0.000
0.000	0.000	1.000	0.000
0.000	0.000	1.250	0.000
0.000	0.000	1.500	0.000
0.000	0.000	1.750	0.000
0.000	0.000	2.000	0.000
0.000	0.000	2.250	0.000
0.000	0.000	2.500	0.000
0.000	0.000	2.750	0.000
0.000	0.000	3.000	0.000
0.000	0.000	3.250	0.000
0.000	0.000	3.500	0.000
0.000	0.000	3.750	0.000
0.000	.024	4.000	.000
0.000	.426	4.250	.003
0.000	1.332	4.500	.010
0.000	3.384	4.750	.024
0.000	7.657	5.000	.055
0.000	12.749	5.250	.092
0.000	16.618	5.500	.120
0.000	19.440	5.750	.140
0.000	20.970	6.000	.151
.006	21.832	6.250	.157
.200	21.066	6.500	.152
.300	17.345	6.750	.125
.600	14.395	7.000	.104
1.100	12.532	7.250	.090
1.700	10.795	7.500	.078
2.500	10.149	7.750	.073
3.500	9.684	8.000	.070
4.600	8.678	8.250	.063
5.800	8.924	8.500	.064
6.500	11.002	8.750	.079
7.600	12.134	9.000	.087
8.500	11.168	9.250	.080
9.700	12.830	9.500	.092
10.800	15.075	9.750	.109
11.600	12.920	10.000	.093
12.100	10.588	10.250	.076
12.600	7.895	10.500	.057
13.000	5.856	10.750	.042
12.400	5.430	11.000	.039
11.600	5.056	11.250	.036
10.700	4.980	11.500	.036
9.900	4.125	11.750	.030
8.900	3.342	12.000	.024
7.900	2.808	12.250	.020
7.700	2.284	12.500	.016
7.500	2.013	12.750	.015
7.700	1.752	13.000	.013
7.900	1.503	13.250	.011
7.700	1.264	13.500	.009
7.500	1.037	13.750	.007
7.300	.810	14.000	.006
7.100	.617	14.250	.004
7.000	.458	14.500	.003

TABLE II. HYDROGRAPH OUTPUT (CONTINUED)

6.700	.323	14.750	.002
6.600	.188	15.000	.001
6.400	.138	15.250	.001
6.200	.101	15.500	.001
5.000	.076	15.750	.001
4.700	.050	16.000	.000
4.400	.025	16.250	.000
4.200	.013	16.500	.000
4.100	0.000	16.750	0.000
3.800	0.000	17.000	0.000
3.500	0.000	17.250	0.000
3.200	0.000	17.500	0.000
3.000	0.000	17.750	0.000
2.900	0.000	18.000	0.000
2.800	0.000	18.250	0.000
2.700	0.000	18.500	0.000
2.600	0.000	18.750	0.000
2.400	0.000	19.000	0.000
2.300	0.000	19.250	0.000
2.200	0.000	19.500	0.000
2.100	0.000	19.750	0.000
2.000	0.000	20.000	0.000
1.800	0.000	20.250	0.000
1.600	0.000	20.500	0.000
1.400	0.000	20.750	0.000
1.300	0.000	21.000	0.000
1.200	0.000	21.250	0.000
1.100	0.000	21.500	0.000
1.000	0.000	21.750	0.000
.900	0.000	22.000	0.000
.800	0.000	22.250	0.000
.800	0.000	22.500	0.000
.800	0.000	22.750	0.000
.800	0.000	23.000	0.000
.800	0.000	23.250	0.000
.750	0.000	23.500	0.000
.710	0.000	23.750	0.000
.650	0.000	24.000	0.000
.610	0.000	24.250	0.000
.610	0.000	24.500	0.000
.600	0.000	24.750	0.000
.550	0.000	25.000	0.000
.470	0.000	25.250	0.000
.470	0.000	25.500	0.000
.470	0.000	25.750	0.000
.470	0.000	26.000	0.000
.470	0.000	26.250	0.000
.470	0.000	26.500	0.000
.470	0.000	26.750	0.000
.470	0.000	27.000	0.000
.470	0.000	27.250	0.000
.470	0.000	27.500	0.000
.430	0.000	27.750	0.000
.400	0.000	28.000	0.000
.370	0.000	28.250	0.000
.330	0.000	28.500	0.000
.320	0.000	28.750	0.000
.300	0.000	29.000	0.000
.290	0.000	29.250	0.000
.280	0.000	29.500	0.000
.280	0.000	29.750	0.000
.270	0.000	30.000	0.000
.260	0.000	30.250	0.000
.240	0.000	30.500	0.000
.240	0.000	30.750	0.000
.240	0.000	31.000	0.000
.240	0.000	31.250	0.000

TABLE II. HYDROGRAPH OUTPUT (CONCLUDED)

.240	0.000	31.500	0.000
.240	0.000	31.750	0.000
.230	0.000	32.000	0.000
.230	0.000	32.250	0.000
.220	0.000	32.500	0.000
.220	0.000	32.750	0.000
.100	0.000	33.000	0.000
.050	0.000	33.250	0.000
0.000	0.000	33.500	0.000

TOTAL SUSPENDED SOLIDS (LBS) DISCHARGED FROM WATERSHED  
DURING STORM EVENT = 2308.209

FE CONC (PPM) 6.80680  
FE LOAD (LBS) 135.87454

MN CONC (PPM) .88400  
MN LOAD (LBS) 17.64604

CA CONC (PPM) 10.82900  
CA LOAD (LBS) 216.16404

MG CONC (PPM) .14277  
MG LOAD (LBS) 2.84984

SO4 CONC (PPM) 5.48080  
SO4 LOAD (LBS) 109.40547

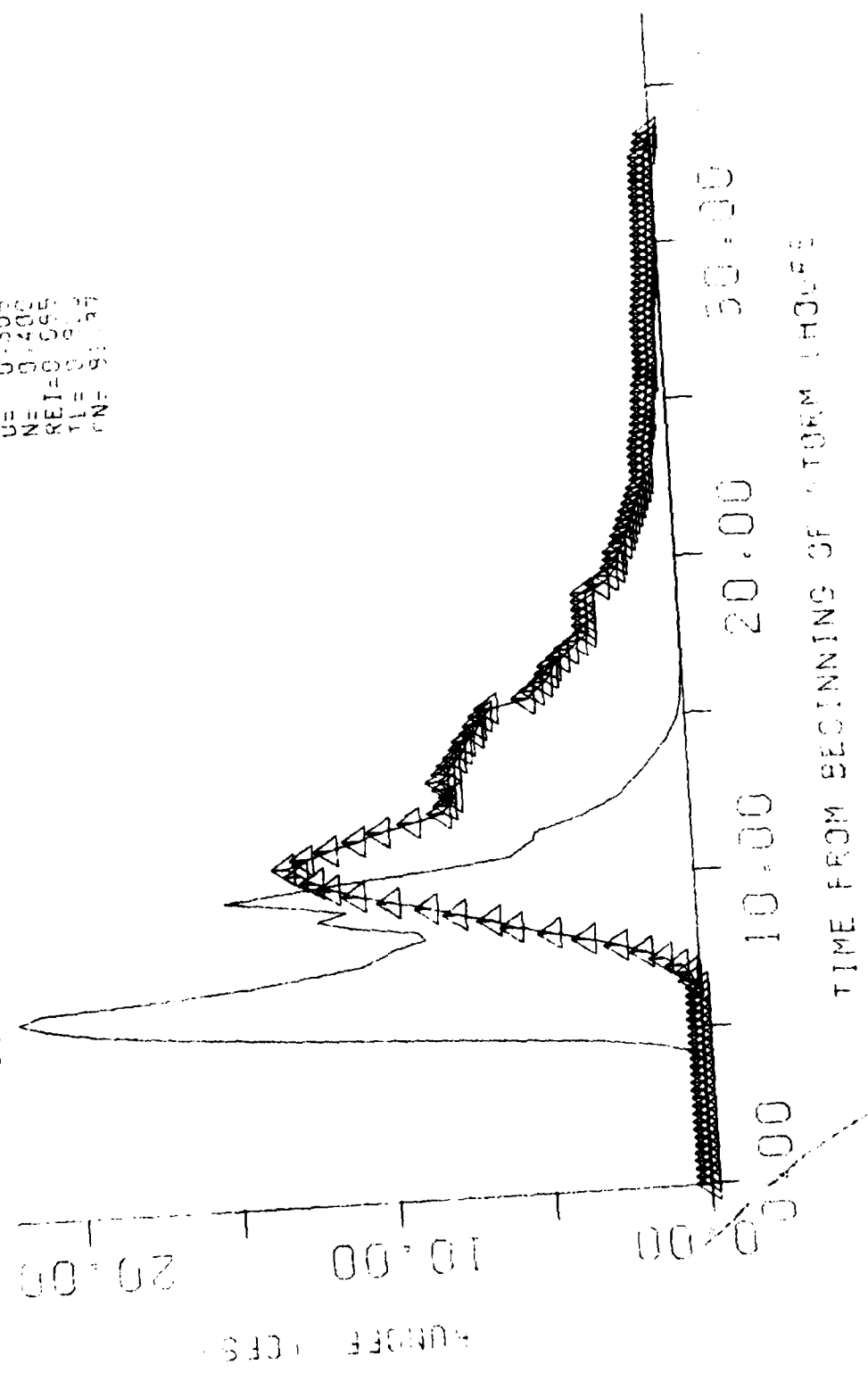
ALK CONC (PPM) 29.65820  
ALK LOAD (LBS) 592.02478

KUP	KT1	KT2	KUR
.663	.632	1.880	.120
U	N	DT	
.306	.400	.25000	

SIMULATED LOAD MODULUS (LBS/AC-IN OF RUNOFF)  
26.16

MCCORMICK  
11-14-78

OBSERVED HYDROGRAPH  
PREDICTED HYDROGRAPH  
U= 0.305  
N= 0.400  
REI=0.505  
YLE=0.000  
CNE= 91.34



## 2. Capehart Marina

An example is provided for the Capehart Marina watershed at Tyndall AFB, Florida. No runoff data is available, and a design storm is supplied. The design storm of interest is 10 inches of rainfall in 12 hours read in at increments of one tenth of an hour. The watershed area is 0.17 square mile with 14.5 percent forest, 1 percent denuded area, and 15 percent impervious area. Curve number 58 was selected from Table 1. The watershed is urban with storm sewers.

A listing of the input and output follows.

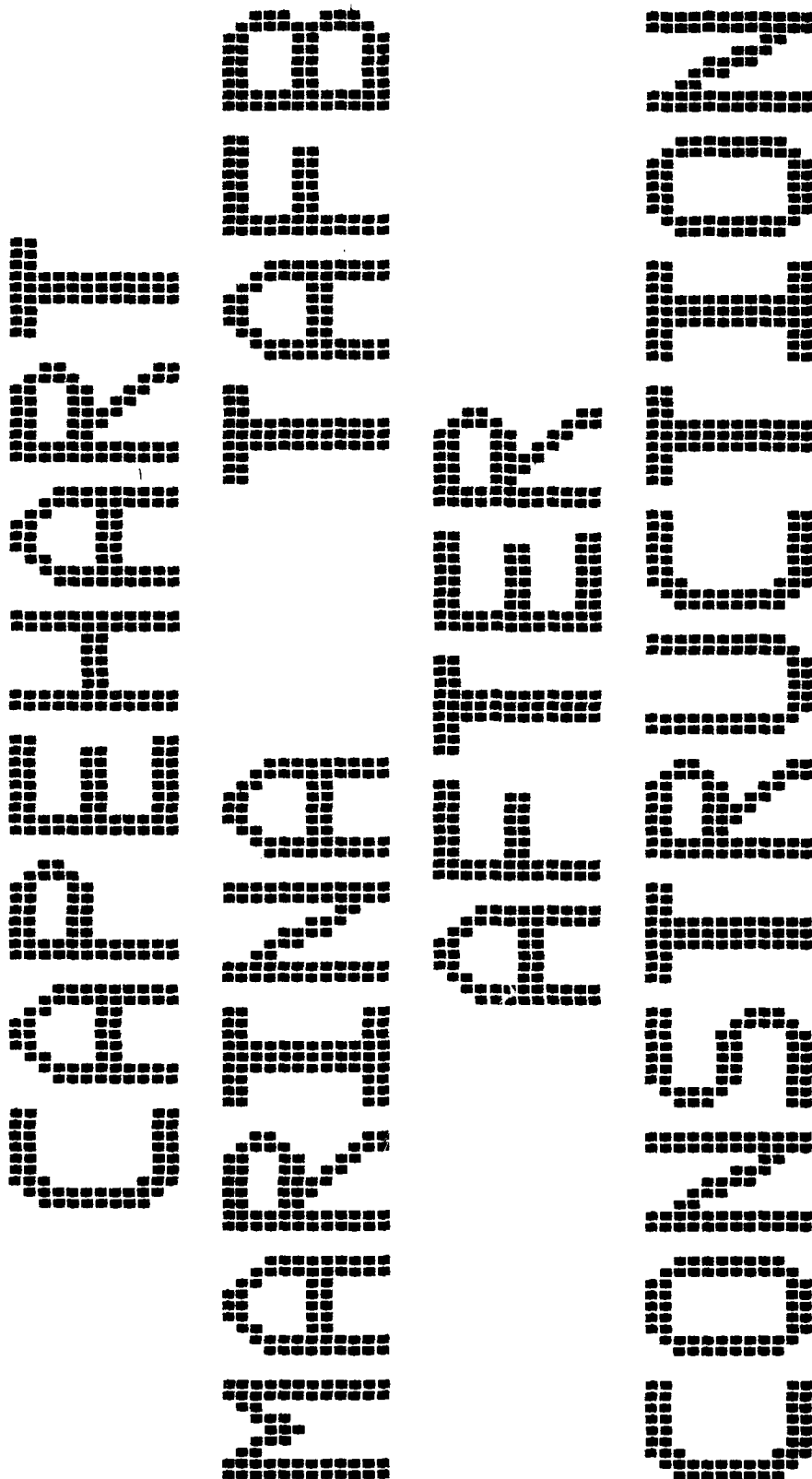
CAPEHART  
 MARINA, TAFB  
 AFTER  
 CONSTRUCTION  
 CAPEHART MARINA AFTER CONSTRUCTION  
 1 1 1 1 1 1  
 .17 14.5 1. 15.  
 58.  
 1  
 CAPEHART MARINA -(AFTER)  
 04-22-80

00.  
 00.05  
 00.1  
 00.15  
 .2  
 .25  
 .3  
 .35  
 .40  
 .5  
 .55  
 .6  
 .65  
 .7  
 .75  
 .80  
 .85  
 .9  
 .95

1.  
 1.1  
 1.2  
 1.3  
 1.4  
 1.5  
 1.6  
 1.7  
 1.8  
 1.9  
 2.0  
 2.1  
 2.2  
 2.3  
 2.4  
 2.5  
 2.6  
 2.7  
 2.8  
 2.9  
 3.0  
 3.1  
 3.2  
 3.3  
 3.4  
 3.5  
 3.6  
 3.7  
 3.8  
 3.9  
 4.0  
 4.1  
 4.2  
 4.3  
 4.4  
 4.5  
 4.6  
 4.7  
 4.8  
 4.9

5.0  
 5.1  
 5.2  
 5.3  
 5.4  
 5.5  
 5.6  
 5.7  
 5.8  
 5.9  
 6.0  
 6.15  
 6.30  
 6.45  
 6.60  
 6.75  
 6.9  
 7.0  
 7.1  
 7.2  
 7.3  
 7.4  
 7.5  
 7.6  
 7.7  
 7.8  
 7.9  
 8.0  
 8.1  
 8.2  
 8.3  
 8.4  
 8.5  
 8.6  
 8.7  
 8.8  
 8.9  
 9.0  
 9.05  
 9.10  
 9.15  
 9.20  
 9.25  
 9.30  
 9.35  
 9.40  
 9.45  
 9.50  
 9.55  
 9.60  
 9.65  
 9.70  
 9.75  
 9.80  
 9.85  
 9.90  
 9.95  
 10.





## INTRODUCTION

THE U.S. AIR FORCE RUNOFF MODEL (AFRUM) FOR SIMULATING STORM HYDROGRAPHS AND POLLUTANT YIELDS WAS DEVELOPED FOR THE AIR FORCE BY THE DEPARTMENT OF CIVIL ENGINEERING, UNIVERSITY OF TENNESSEE, KNOXVILLE AND THE RESEARCH AND DEVELOPMENT DIRECTORATE OF THE AIR FORCE ENGINEERING SERVICES CENTER (AFESC), TYNDALL AIR FORCE BASE, FLORIDA. DR. DONALD E. OVERTON OF THE UNIVERSITY OF TENNESSEE WAS THE PRINCIPAL INVESTIGATOR AND DR. GEORGE W. SCHLOSSNAGLE OF THE U.S. AIR FORCE WAS THE PROJECT OFFICER. THE RESULTS OF THREE SEPARATE BUT COMPLIMENTARY STUDIES WERE INCORPORATED INTO AFRUM. EACH OF THE THREE STUDIES HAD THE FUNDAMENTAL OBJECTIVE TO EVALUATE THE EFFECTS OF SPECIALIZED LAND USE ON STORMWATER RUNOFF AND ITS ASSOCIATED QUALITY. THE THREE STUDIES WERE FUNDED BY THE U.S. DEPARTMENT OF ENERGY, THE U.S. DEPARTMENT OF INTERIOR AND THE U.S. AIR FORCE. THE STUDY PERIOD WAS FROM 1975 THROUGH 1979. AFRUM WAS DEVELOPED IN THE COURSE OF ANALYZING 410 STORM EVENTS ON 36 WATERSHEDS, WHICH INCLUDED AGRICULTURAL, URBAN AND FORESTED LAND USE CONDITIONS AS WELL AS COAL STRIP MINING AND THREE WATERSHEDS ON A U.S. AIR FORCE BASE.

AFRUM WAS DEVELOPED FOR THE PURPOSE OF SIMULATING STORMWATER HYDROGRAPHS FROM ACTUAL OR DESIGN STORM RAINFALL DISTRIBUTIONS, LAND USE CHARACTERISTICS AND SOIL TYPE IN THE WATERSHED OF CONCERN. THE REQUIRED INPUT BASIN CHARACTERISTICS ARE:

1. PERCENT OF WATERSHED THAT IS FORESTED
2. PERCENT OF WATERSHED THAT IS IMPERVIOUS
3. PERCENT OF WATERSHED THAT IS DENUDED OR STRIP MINED
4. SURFACE DRAINAGE AREA

RUNOFF VOLUME AND THE ASSOCIATED RAINFALL EXCESS TIME DISTRIBUTION ARE SIMULATED FROM INPUT RAINFALL USING THE U.S. SOIL CONSERVATION SERVICE CURVE NUMBER. IF A RUNOFF HYDROGRAPH IS PROVIDED WITH THE ASSOCIATED RAINFALL HYETOGRAPH, AFRUM WILL COMPUTE THE CURVE NUMBER, CN; OTHERWISE CN MUST BE AN INPUT. CN IS SELECTED BY USING THE PROCEDURES PROVIDED IN THE NATIONAL ENGINEERING HANDBOOK, SECTION 4, U.S. SOIL CONSERVATION SERVICE.

AFRUM MAKES PROVISION FOR SIMULATING A UNIT HYDROGRAPH OR UNIT RESPONSE FUNCTION, WHICH IS CONVOLUTED WITH THE RAINFALL EXCESS HYETOGRAPH. AFRUM ALSO SIMULATES POLLUTANT LOADS FOR THE INPUTED STORM. THIS SIMULATION IS A FUNCTION OF THE SPECIFIED WATERSHED AND STORM CHARACTERISTICS.

# CAPEHART MARINA AFTER CONSTRUCTION

THE WATERSHED NAME IS CAPEHART MARINA -(AFTER)  
THE DATE OF THE RAINFALL EVENT IS 04-22-80  
THE WATERSHED SIZE IN SQUARE MILES IS: SQMI= .17  
THE PERCENT OF THE BASIN WHICH IS FOREST IS: PF= 14.50  
THE PERCENT OF THE BASIN DENUDED IS: PS= 1.00  
THE PERCENT OF THE BASIN WHICH IS IMPERVIOUS IS: PI= 15.00

BY SETTING ISIM = 1 YOU HAVE INDICATED THAT YOU PLAN  
TO SUPPLY ACTUAL OR DESIGN RAINFALL DATA; THEREFORE, AN  
ESTIMATE OF THE SCS CURVE NUMBER, CN, MUST BE PROVIDED.

OUTPUT UNITS OF THE SIMULATED HYDROGRAPH ARE HOURS  
AND CUBIC FEET PER SECOND, CFS, AS SELECTED BY SETTING  
IUNIT = 1.

YOU HAVE REQUESTED THAT THE HYDROGRAPH BE PLOTTED  
BY SETTING IPLOT = 1.

THE WATERSHED IS ASSUMED TO BE URBAN WITH STORM  
SEWERS; ICHAR = 1.

YOU HAVE ELECTED TO SIMULATE LAG MODULUS IN  
HOURS ASSUMING IT IS A FUNCTION OF THE WATERSHED AREA  
AND PERCENT IMPERVIOUS AREA OF THE WATERSHED; ILAG = 1.

SEDIMENT LOAD HAS BEEN SIMULATED ASSUMING THE  
WATERSHED IS RURAL OR URBAN WITHOUT MAJOR CONSTRUCTION;  
ILOAD = 1.

TABLE I. USER INPUT

TIME (HR)	TOTAL RAIN (IN)	INCREMENTAL RAIN (IN)	OBSERVED FLOW (CFS)	DATA FLOW (IN/HR)
0.00	0.00	0.00	0.00	0.000000
.10	.05	.05	0.00	0.000000
.20	.10	.05	0.00	0.000000
.30	.15	.05	0.00	0.000000
.40	.20	.05	0.00	0.000000
.50	.25	.05	0.00	0.000000
.60	.30	.05	0.00	0.000000
.70	.35	.05	0.00	0.000000
.80	.40	.05	0.00	0.000000
.90	.50	.10	0.00	0.000000
1.00	.55	.05	0.00	0.000000
1.10	.60	.05	0.00	0.000000
1.20	.65	.05	0.00	0.000000
1.30	.70	.05	0.00	0.000000
1.40	.75	.05	0.00	0.000000
1.50	.80	.05	0.00	0.000000
1.60	.85	.05	0.00	0.000000
1.70	.90	.05	0.00	0.000000
1.80	.95	.05	0.00	0.000000
1.90	1.00	.05	0.00	0.000000
2.00	1.10	.10	0.00	0.000000
2.10	1.20	.10	0.00	0.000000
2.20	1.30	.10	0.00	0.000000
2.30	1.40	.10	0.00	0.000000
2.40	1.50	.10	0.00	0.000000
2.50	1.60	.10	0.00	0.000000
2.60	1.70	.10	0.00	0.000000
2.70	1.80	.10	0.00	0.000000
2.80	1.90	.10	0.00	0.000000
2.90	2.00	.10	0.00	0.000000
3.00	2.10	.10	0.00	0.000000
3.10	2.20	.10	0.00	0.000000
3.20	2.30	.10	0.00	0.000000
3.30	2.40	.10	0.00	0.000000
3.40	2.50	.10	0.00	0.000000
3.50	2.60	.10	0.00	0.000000
3.60	2.70	.10	0.00	0.000000
3.70	2.80	.10	0.00	0.000000
3.80	2.90	.10	0.00	0.000000
3.90	3.00	.10	0.00	0.000000
4.00	3.10	.10	0.00	0.000000
4.10	3.20	.10	0.00	0.000000
4.20	3.30	.10	0.00	0.000000
4.30	3.40	.10	0.00	0.000000
4.40	3.50	.10	0.00	0.000000
4.50	3.60	.10	0.00	0.000000
4.60	3.70	.10	0.00	0.000000
4.70	3.80	.10	0.00	0.000000
4.80	3.90	.10	0.00	0.000000
4.90	4.00	.10	0.00	0.000000
5.00	4.10	.10	0.00	0.000000
5.10	4.20	.10	0.00	0.000000
5.20	4.30	.10	0.00	0.000000
5.30	4.40	.10	0.00	0.000000
5.40	4.50	.10	0.00	0.000000
5.50	4.60	.10	0.00	0.000000
5.60	4.70	.10	0.00	0.000000
5.70	4.80	.10	0.00	0.000000
5.80	4.90	.10	0.00	0.000000
5.90	5.00	.10	0.00	0.000000

6.00	5.10	.10	0.00	0.000000
6.10	5.20	.10	0.00	0.000000
6.20	5.30	.10	0.00	0.000000
6.30	5.40	.10	0.00	0.000000
6.40	5.50	.10	0.00	0.000000
6.50	5.60	.10	0.00	0.000000
6.60	5.70	.10	0.00	0.000000
6.70	5.80	.10	0.00	0.000000
6.80	5.90	.10	0.00	0.000000
6.90	6.00	.10	0.00	0.000000
7.00	6.15	.15	0.00	0.000000
7.10	6.30	.15	0.00	0.000000
7.20	6.45	.15	0.00	0.000000
7.30	6.60	.15	0.00	0.000000
7.40	6.75	.15	0.00	0.000000
7.50	6.90	.15	0.00	0.000000
7.60	7.00	.10	0.00	0.000000
7.70	7.10	.10	0.00	0.000000
7.80	7.20	.10	0.00	0.000000
7.90	7.30	.10	0.00	0.000000
8.00	7.40	.10	0.00	0.000000
8.10	7.50	.10	0.00	0.000000
8.20	7.60	.10	0.00	0.000000
8.30	7.70	.10	0.00	0.000000
8.40	7.80	.10	0.00	0.000000
8.50	7.90	.10	0.00	0.000000
8.60	8.00	.10	0.00	0.000000
8.70	8.10	.10	0.00	0.000000
8.80	8.20	.10	0.00	0.000000
8.90	8.30	.10	0.00	0.000000
9.00	8.40	.10	0.00	0.000000
9.10	8.50	.10	0.00	0.000000
9.20	8.60	.10	0.00	0.000000
9.30	8.70	.10	0.00	0.000000
9.40	8.80	.10	0.00	0.000000
9.50	8.90	.10	0.00	0.000000
9.60	9.00	.10	0.00	0.000000
9.70	9.05	.05	0.00	0.000000
9.80	9.10	.05	0.00	0.000000
9.90	9.15	.05	0.00	0.000000
10.00	9.20	.05	0.00	0.000000
10.10	9.25	.05	0.00	0.000000
10.20	9.30	.05	0.00	0.000000
10.30	9.35	.05	0.00	0.000000
10.40	9.40	.05	0.00	0.000000
10.50	9.45	.05	0.00	0.000000
10.60	9.50	.05	0.00	0.000000
10.70	9.55	.05	0.00	0.000000
10.80	9.60	.05	0.00	0.000000
10.90	9.65	.05	0.00	0.000000
11.00	9.70	.05	0.00	0.000000
11.10	9.75	.05	0.00	0.000000
11.20	9.80	.05	0.00	0.000000
11.30	9.85	.05	0.00	0.000000
11.40	9.90	.05	0.00	0.000000
11.50	9.95	.05	0.00	0.000000
11.60	10.00	.05	0.00	0.000000

ESTIMATED CN= 58.00

RFI	U	N	TL	UP	UR	T1	T2	T3	AREA
.600	.220	.400	.270	3.330	.129	.300	.500	2.900	1.001

ADJUSTED HYDROGRAPH PARAMETERS

UP	UR	T1	T2	T3	AREA
3.327	.129	.300	.500	2.900	1.000

TABLE II. HYDROGRAPH OUTPUT

OBSERVED FLOW OUT OF WATERSHED (CFS)	PREDICTED FLOW OUT OF WATERSHED (CFS)	TIME (HOURS)	SUSPENDED SOLIDS DISCHARGED FROM WATERSHED LBS/SEC
0.000	0.000	0.000	0.000
0.000	0.000	.100	0.000
0.000	0.000	.200	0.000
0.000	0.000	.300	0.000
0.000	0.000	.400	0.000
0.000	0.000	.500	0.000
0.000	0.000	.600	0.000
0.000	0.000	.700	0.000
0.000	0.000	.800	0.000
0.000	0.000	.900	0.000
0.000	0.000	1.000	0.000
0.000	0.000	1.100	0.000
0.000	0.000	1.200	0.000
0.000	0.000	1.300	0.000
0.000	0.000	1.400	0.000
0.000	0.000	1.500	0.000
0.000	0.000	1.600	0.000
0.000	0.000	1.700	0.000
0.000	0.000	1.800	0.000
0.000	0.000	1.900	0.000
0.000	0.000	2.000	0.000
0.000	0.000	2.100	0.000
0.000	0.000	2.200	0.000
0.000	0.000	2.300	0.000
0.000	0.000	2.400	0.000
0.000	.045	2.500	.000
0.000	.423	2.600	.001
0.000	1.452	2.700	.004
0.000	3.326	2.800	.009
0.000	5.628	2.900	.016
0.000	7.932	3.000	.023
0.000	10.184	3.100	.029
0.000	12.384	3.200	.035
0.000	14.534	3.300	.041
0.000	16.636	3.400	.047
0.000	18.690	3.500	.053
0.000	20.698	3.600	.059
0.000	22.659	3.700	.064
0.000	24.576	3.800	.070
0.000	26.449	3.900	.075
0.000	28.278	4.000	.080
0.000	30.064	4.100	.085
0.000	31.807	4.200	.090
0.000	33.509	4.300	.095
0.000	35.169	4.400	.100
0.000	36.787	4.500	.104
0.000	38.365	4.600	.109
0.000	39.901	4.700	.113
0.000	41.398	4.800	.117
0.000	42.853	4.900	.122
0.000	44.269	5.000	.126
0.000	45.644	5.100	.129
0.000	46.980	5.200	.133
0.000	48.275	5.300	.137
0.000	49.531	5.400	.141
0.000	50.749	5.500	.144

0.0000	51.930	5.600	.147
0.0000	53.075	5.700	.151
0.0000	54.187	5.800	.154
0.0000	55.266	5.900	.157
0.0000	56.314	6.000	.160
0.0000	57.332	6.100	.163
0.0000	58.321	6.200	.165
0.0000	59.282	6.300	.168
0.0000	60.217	6.400	.171
0.0000	61.125	6.500	.173
0.0000	62.009	6.600	.176
0.0000	62.869	6.700	.178
0.0000	63.705	6.800	.181
0.0000	64.520	6.900	.183
0.0000	65.313	7.000	.185
0.0000	69.922	7.100	.198
0.0000	78.443	7.200	.223
0.0000	90.962	7.300	.258
0.0000	98.196	7.400	.279
0.0000	99.998	7.500	.284
0.0000	101.745	7.600	.289
0.0000	99.296	7.700	.282
0.0000	92.577	7.800	.263
0.0000	81.518	7.900	.231
0.0000	76.166	8.000	.216
0.0000	76.637	8.100	.217
0.0000	77.093	8.200	.219
0.0000	77.535	8.300	.220
0.0000	77.963	8.400	.221
0.0000	78.378	8.500	.222
0.0000	78.780	8.600	.224
0.0000	79.169	8.700	.225
0.0000	79.546	8.800	.226
0.0000	79.911	8.900	.227
0.0000	80.264	9.000	.228
0.0000	80.606	9.100	.229
0.0000	80.937	9.200	.230
0.0000	81.258	9.300	.231
0.0000	81.568	9.400	.231
0.0000	81.868	9.500	.232
0.0000	82.158	9.600	.233
0.0000	82.439	9.700	.234
0.0000	78.070	9.800	.221
0.0000	69.023	9.900	.196
0.0000	55.288	10.000	.157
0.0000	48.170	10.100	.137
0.0000	47.711	10.200	.135
0.0000	47.289	10.300	.134
0.0000	46.903	10.400	.133
0.0000	46.554	10.500	.132
0.0000	46.223	10.600	.131
0.0000	45.910	10.700	.130
0.0000	45.616	10.800	.129
0.0000	45.340	10.900	.129
0.0000	45.083	11.000	.128
0.0000	44.845	11.100	.127
0.0000	44.626	11.200	.127
0.0000	44.426	11.300	.126
0.0000	44.246	11.400	.126
0.0000	44.086	11.500	.125
0.0000	43.946	11.600	.125
0.0000	43.826	11.700	.124
0.0000	38.918	11.800	.110
0.0000	29.213	11.900	.083
0.0000	14.705	12.000	.042
0.0000	7.127	12.100	.020
0.0000	6.490	12.200	.018
0.0000	5.897	12.300	.017
0.0000	5.349	12.400	.015
0.0000	4.845	12.500	.014



0.000	4.387	12.600	.012
0.000	3.950	12.700	.011
0.000	3.537	12.800	.010
0.000	3.146	12.900	.009
0.000	2.777	13.000	.008
0.000	2.432	13.100	.007
0.000	2.109	13.200	.006
0.000	1.809	13.300	.005
0.000	1.531	13.400	.004
0.000	1.277	13.500	.004
0.000	1.045	13.600	.003
0.000	.837	13.700	.002
0.000	.651	13.800	.002
0.000	.489	13.900	.001
0.000	.349	14.000	.001
0.000	.233	14.100	.001
0.000	.140	14.200	.000
0.000	.070	14.300	.000
0.000	.023	14.400	.000
0.000	0.000	14.500	0.000

TOTAL SUSPENDED SOLIDS (LBS) DISCHARGED FROM WATERSHED  
DURING STORM EVENT = 5188.523

FE CONC (PPM) 6.80680  
FE LOAD (LBS) 775.87097

MN CONC (PPM) .88400  
MN LOAD (LBS) 100.76246

CA CONC (PPM) 10.82900  
CA LOAD (LBS) 1234.34018

MG CONC (PPM) .14277  
MG LOAD (LBS) 16.27314

SO4 CONC (PPM) 5.48080  
SO4 LOAD (LBS) 624.72727

ALK CONC (PPM) 29.65820  
ALK LOAD (LBS) 3380.58065

OPTIMIZED CURVE NUMBER = 0.0

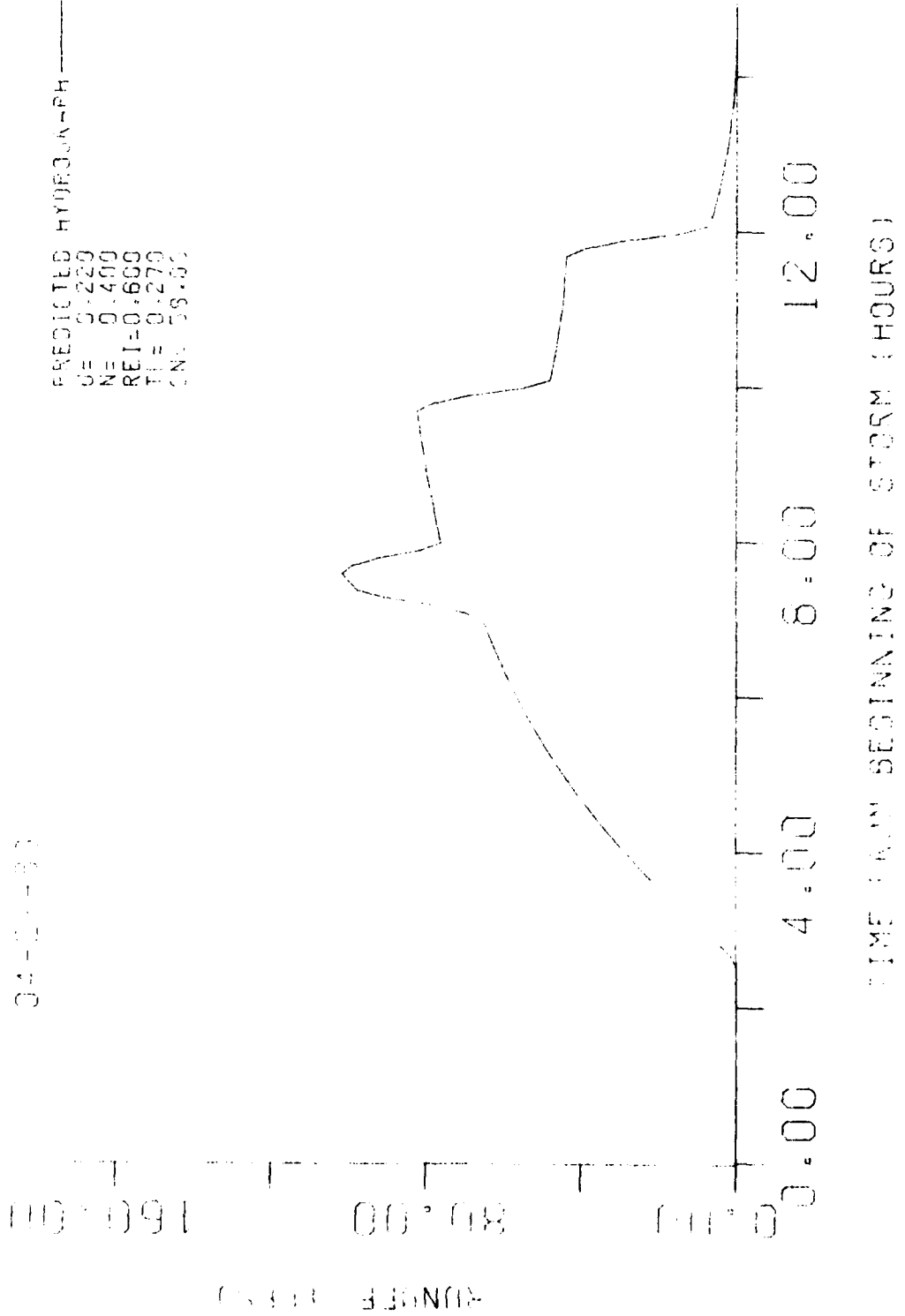
TOTAL RUNOFF= 4.6306INCHES

KUP	KT1	KT2	KUR
.900	.956	1.800	.035
U	N	DT	
.220	.400	.10000	

SIMULATED LOAD MODULUS (LBS/AC-IN OF RUNOFF)  
10.30

COASTAL WINDING - AFTER  
04-00-00

PREDICTED HYDROGRAPH  
GE = 0.220  
NE = 0.400  
REI = 0.600  
TE = 0.270  
CN = 0.800



#### REFERENCES

1. U.S. Soil Conservation Service, National Engineering Handbook Section 4, Hydrology, Washington, D.C., 1972.
2. Ardis, C.V., Jr., "Storm Hydrographs Using a Double Triangle Model," TVA, Division of Water Control Planning, January 1973.
3. Betson, R.P., Urban Hydrology - A Systems Study in Knoxville, Tennessee, TVA, Division of Water Management, 1976.
4. Overton, D.E., W.L. Troxler and E.C. Crosby, "Simulation of Effects of Urbanization of Stormwater Runoff and Quality," Univ. of Tennessee, Water Resource Center, Report No. 74, December 1979.
5. Overton, D.E., and E.C. Crosby, "Effects of Contour Coal Strip Mining on Stormwater Runoff and Quality - New River Basin, Tennessee," Department of Civil Engineering, The University of Tennessee, Knoxville, 1979.
6. Overton, D.E. and M.E. Meadows, Stormwater Modeling, Academic Press Inc., New York, 1976.

APPENDIX A  
LISTING OF AFRUM

```

1  PROGRAM AFRUM (INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,TAPE7,TAPE9)
5
10
15
20
25
30
35
40
45
50
55
60

```



```

135      NO. OF RAINFALL/RUNOFF CARDS MUST BE EQUAL TO NUMBER OF RAINFALL/RUNOFF
140      OBSERVATIONS
145      A MAXIMUM OF 500 RAINFALL/RUNOFF OBSERVATIONS MAY BE SUBMITTED
150      *****
155      REAL KT1,KT2,KUP,IMP,LOSS,KT23,KUR
160      COMMON RUNOFF(800),HYDRO(800),RNOFF(500),RAIN(500),STAGE(500)
165      >AREA(500),RF(500),PE(500),PE(500),SRO(500),BASIN(4),BDAYE,
170      >IAREA(664),PHI,DT,U,T1,T2,T3,UP,UR,REI,KT1,KT2,KUP,RN,ITOTAL,
175      >ICHASH,IDMAX,NPRF,UMHYDRO(800),NPRO,CNOPT,NBIC,TL,KT23,
180      >TIME(500),TFLOW(500),TFLOWI(500),SFLOW(500),BSFLOW(500)
185      >DUMX(4),DUMY(4),BIGX,OBPEAK,PRPEAK,TP08,TPPR,ISIM
190      >IPL0T,IUNIT,NPRF1,NPRE2,AREA,KUR
195      >ITL(20),SQMI,SHAPE,SC,DD,SINU,CNA,SS,IMP,TLP
200      <<LOAD,DL0AD
205      *****
210      THE FOLLOWING DATA CARDS CONTAIN COEFFICIENTS FOR SIMULATING LAG MODULUS,
215      UP, T1, T2, AND T3 US A FUNCTION OF WATERSHED CHARACTERISTICS.
220      THESE REGIONALIZED COEFFICIENTS WERE DERIVED BY USING BMDP4R (LINEAR
225      REGRESSION UPON PRINCIPAL COMPONENTS).
230      THESE COEFFICIENTS ARE SUBJECT TO REVISION AS MORE DATA BECOMES AVAILABLE
235      *****
240      DATA C1,C2,C3,C4,C5,C6,C7,C8,C9,C10,-8.4076,0.0133,0.5126,0.0001,
245      >-0.0635,7.2776,0.0333,0.0794,1.7401,-2.0510,
250      >DATA C11,C12,C13,C14,C15,C16,C17,C18,C19,C20,0.4466,0.0019,-0.015
255      >1,-0.0001,0.0066,-0.0312,0.0007,0.0018,0.2213,0.07726,
260      >DATA C21,C22,C23,C24,C25,C26,C27,C28,C29,C30,0.2989,0.0066,-0.058
265      >9,-0.0002,0.0157,-0.2129,-0.0031,0.0017,0.3455,-0.4254,
270      >DATA C31,C32,C33,C34,C35,C36,C37,C38,C39,C40,0.7129,0.0063,-0.040
275      >1,0.000,0.0264,0.3054,-0.0018,0.0138,-0.3646,-0.0733,
280      >DATA C41,C42,C43,C44,C45,C46,C47,C48,C49,C50,-3.9713,-0.0208,0.394
285      >8,0.0,-0.0156,1.9912,0.0051,0.0284,9.27258,1.18497/
290      CALL PLOT(0.0,1.5,-3)
295      PRINTS BANNER ( FIRST 4 CRDS)
300      CALL LETTER
305      CALL AESOP
310      IDMAX=MAXIMUM DIMENSION OF MATRIX HYDRO
315      IDMAX=800
320      READ WATERSHED LOCATION AND NAME (CARD 1)
325      READ(5,9) TITLE
330      FORMAT(20A4)
335      FORMAT (4A10)
340      READ PROGRAM CONTROL PARAMETERS (CARD 2)
345      READ(5,12) ISIM,IUNIT,IPL0T,ICHAR,ILAG,ILOAD
350      FORMAT(16I4)
355      READ WATERSHED PHYSICAL CHARACTERISTICS (CARD 3)
360      READ(5,14) SQMI,PF,PS,PI
365      FORMAT(4F8.2)
370      IF (ISIM.EQ.2) GO TO 16
375      READ SCS CURVE NUMBER (CARD 4)
380      READ(5,15) CN
385      FORMAT(F10.0)
390      *****
395      AFRUM 137
396      AFRUM 138
397      AFRUM 139
398      AFRUM 140
399      AFRUM 141
400      AFRUM 142
401      AFRUM 143
402      AFRUM 144
403      AFRUM 145
404      AFRUM 146
405      AFRUM 147
406      AFRUM 148
407      AFRUM 149
408      AFRUM 150
409      AFRUM 151
410      AFRUM 152
411      AFRUM 153
412      AFRUM 154
413      AFRUM 155
414      AFRUM 156
415      AFRUM 157
416      AFRUM 158
417      AFRUM 159
418      AFRUM 160
419      AFRUM 161
420      AFRUM 162
421      AFRUM 163
422      AFRUM 164
423      AFRUM 165
424      AFRUM 166
425      AFRUM 167
426      AFRUM 168
427      AFRUM 169
428      AFRUM 170
429      AFRUM 171
430      AFRUM 172
431      AFRUM 173
432      AFRUM 174
433      AFRUM 175
434      AFRUM 176
435      AFRUM 177
436      AFRUM 178
437      AFRUM 179
438      AFRUM 180
439      AFRUM 181
440      AFRUM 182
441      AFRUM 183
442      AFRUM 184
443      AFRUM 185
444      AFRUM 186
445      AFRUM 187
446      AFRUM 188
447      AFRUM 189
448      AFRUM 190
449      AFRUM 191
450      AFRUM 192
451      AFRUM 193
452      AFRUM 194
453      AFRUM 195
454      AFRUM 196
455      AFRUM 197
456      AFRUM 198
457      AFRUM 199
458      AFRUM 200
459      AFRUM 201
460      AFRUM 202
461      AFRUM 203
462      AFRUM 204
463      AFRUM 205

```

205	16	CONTINUE	AFRUM
	C	RN=.	AFRUM
	C	HEAD LAG MODULUS (CARD 5)	AFRUM
210	C	IF (LAG.GT. 0) GO TO 20	AFRUM
		READ(15,1) U	AFRUM
		GO TO 23	AFRUM
215	20	IF (LAG.EQ. 1) GO TO 22	AFRUM
		U=(0.660+SOMI)+(0.0203*PF) * 1.16	AFRUM
		IF (U.GE.0.0) GO TO 23	AFRUM
		WRITE(6,520)	AFRUM
520	520	FORMAT(5X,"NEGATIVE VALUE OF LAGMODULUS SIMULATED,PROGRAM STOPPED >."/)	AFRUM
		IQUIT=1	AFRUM
220	22	GO TO 23	AFRUM
		U=3.24*(SOMI/PI)**0.6	AFRUM
		IF (U.GE. 0.0) GO TO 23	AFRUM
		WRITE(6,21)	AFRUM
225	21	FORMAT(5X,"NEGATIVE VALUE OF LAGMODULUS SIMULATED,PROGRAM STOPPED >."/)	AFRUM
		IQUIT=1	AFRUM
23	23	CONTINUE	AFRUM
	C	DEFINE NORMALIZED UNIT RESPONSE FUNCTION	AFRUM
230	C	IF (ICHR .GT. 0) GO TO 24	AFRUM
		KUP=0.663	AFRUM
		KT1=0.632	AFRUM
		KT2=1.88	AFRUM
235		KUR=0.12	AFRUM
		GO TO 30	AFRUM
		IF (ICHR .GT. 1) GO TO 25	AFRUM
24	24	KUP=0.900	AFRUM
		KT1=0.956	AFRUM
		KT2=1.80	AFRUM
		KUR=0.035	AFRUM
		GO TO 30	AFRUM
		.GT. 2) GO TO 26	AFRUM
25	25	IF (ICHR	AFRUM
		KUP=0.253	AFRUM
		KT1=0.283	AFRUM
		KT2=1.021	AFRUM
		KUR=0.21	AFRUM
		GO TO 30	AFRUM
		IF (ICHR	AFRUM
		KUP=0.705	AFRUM
		KT1=0.695	AFRUM
		KT2=1.87	AFRUM
		KUR=0.13	AFRUM
		GO TO 30	AFRUM
255	27	KUP=0.716	AFRUM
		KT1=0.394	AFRUM
		KT2=1.57	AFRUM
		KUR=0.10	AFRUM
		CONTINUE	AFRUM
260	30	READ TIME INTERVAL (CARD 6)	AFRUM
	C	READ(15,15) DT	AFRUM
		IF (ILOAD.EQ. 1) DLOAD=16.7*PS-21.5*U*PF+62.3	AFRUM
		IF (ILOAD.EQ. 2) DLOAD=18.17*PS-1.28*U*PF+52.7	AFRUM
265		IF (DLOAD.GT. 0.0) GO TO 36	AFRUM
		DLOAD = 0.0	AFRUM
		WRITE (6,31)	AFRUM
		FORMAT (1H ,/,/,12X,"WARNING: EQUATIONS PREDICT MORE SEDIMENT CAN	AFRUM
31	31		AFRUM





```

347 IF (ISIM .EQ. 1) PHI=0.0
348 IF (ISIM .EQ. 1) GO TO 290
349 DO 160 I=1,NPRO
350 TRUN=TRUN+RNOFF(I)
351 CONTINUE
352 IF (TRUN .LE. RAIN(NPRF)) GO TO 165
353 WRITE(6,162)
354 FORMAT(1X,"APPARENT ERROR IN DATA: RUNOFF EXCEEDS RAINFALL"/
355 >5X,"POSSIBLE CAUSE",25X,"CORRECTIVE ACTION"/
356 >1X,"(1)",2X,"NONUNIFORM RAINFALL DISTRIBUTION",7X,"DISCARD DATA"/
357 >1X,"(2)",2X,"ESTIMATE OF CN IS TOO LARGE",12X,"REDUCE INPUT CN"/)
358 GO TO 460
359 LOSS=RMAX-TRUN
360 RFINTR=RMAX/((NPRF-1)*DT)
361 CNL=10.0
362 CNR=100.0
363 CNM=(CNL+CNR)/2.0
364 CALL SCS(CNL)
365 PRUNL=SRO(NPRF)
366 CALL SCS(CNR)
367 PRUNR=SRO(NPRF)
368 CALL SCS(CNM)
369 PRUNM=SRO(NPRF)
370 DP=PRUNM-TRUN
371 IF (DP<0.0) 240,270,220
372 CNR=CNM+DP
373 CNL=CNM-DP
374 GO TO 160
375 CNL=CNM
376 CNR=CNM
377 CNM=CNL
378 CNM=CNR
379 CNM=CNL
380 CNM=CNR
381 CNM=CNL
382 CNM=CNR
383 CNM=CNL
384 CNM=CNR
385 CNM=CNL
386 CNM=CNR
387 CNM=CNL
388 CNM=CNR
389 CNM=CNL
390 CNM=CNR
391 CNM=CNL
392 CNM=CNR
393 CNM=CNL
394 CNM=CNR
395 CNM=CNL
396 CNM=CNR
397 CNM=CNL
398 CNM=CNR
399 CNM=CNL
400 CNM=CNR
401 CNM=CNL
402 CNM=CNR
403 CNM=CNL
404 CNM=CNR
405 CNM=CNL
406 CNM=CNR
407 CNM=CNL
408 CNM=CNR
409 CNM=CNL
410 CNM=CNR

```

[illegible]

SUBROUTINE SCS	74/74	OPT=1	FTN 4.8*518	10/06/80	09.37.33
----------------	-------	-------	-------------	----------	----------

```

1      C
2      C
3      C
4      C
5      C
6      C
7      C
8      C
9      C
10     C
11     C
12     C
13     C
14     C
15     C
16     C
17     C
18     C
19     C
20     C
21     C
22     C
23     C
24     C
25     C
26     C
27     C
28     C
29     C
30     C
31     C
32     C
33     C
34     C
35     C
36     C
37     C
38     C
39     C
40     C
41     C
42     C
43     C
44     C
45     C
46     C
47     C
48     C
49     C
50     C
51     C
52     C
53     C
54     C
55     C
56     C
57     C
58     C
59     C
60     C
61     C
62     C
63     C
64     C
65     C
66     C
67     C
68     C
69     C
70     C
71     C
72     C
73     C
74     C
75     C
76     C
77     C
78     C
79     C
80     C
81     C
82     C
83     C
84     C
85     C
86     C
87     C
88     C
89     C
90     C
91     C
92     C
93     C
94     C
95     C
96     C
97     C
98     C
99     C
100    C
101    C
102    C
103    C
104    C
105    C
106    C
107    C
108    C
109    C
110    C
111    C
112    C
113    C
114    C
115    C
116    C
117    C
118    C
119    C
120    C
121    C
122    C
123    C
124    C
125    C
126    C
127    C
128    C
129    C
130    C
131    C
132    C
133    C
134    C
135    C
136    C
137    C
138    C
139    C
140    C
141    C
142    C
143    C
144    C
145    C
146    C
147    C
148    C
149    C
150    C
151    C
152    C
153    C
154    C
155    C
156    C
157    C
158    C
159    C
160    C
161    C
162    C
163    C
164    C
165    C
166    C
167    C
168    C
169    C
170    C
171    C
172    C
173    C
174    C
175    C
176    C
177    C
178    C
179    C
180    C
181    C
182    C
183    C
184    C
185    C
186    C
187    C
188    C
189    C
190    C
191    C
192    C
193    C
194    C
195    C
196    C
197    C
198    C
199    C
200    C
201    C
202    C
203    C
204    C
205    C
206    C
207    C
208    C
209    C
210    C
211    C
212    C
213    C
214    C
215    C
216    C
217    C
218    C
219    C
220    C
221    C
222    C
223    C
224    C
225    C
226    C
227    C
228    C
229    C
230    C
231    C
232    C
233    C
234    C
235    C
236    C
237    C
238    C
239    C
240    C
241    C
242    C
243    C
244    C
245    C
246    C
247    C
248    C
249    C
250    C
251    C
252    C
253    C
254    C
255    C
256    C
257    C
258    C
259    C
260    C
261    C
262    C
263    C
264    C
265    C
266    C
267    C
268    C
269    C
270    C
271    C
272    C
273    C
274    C
275    C
276    C
277    C
278    C
279    C
280    C
281    C
282    C
283    C
284    C
285    C
286    C
287    C
288    C
289    C
290    C
291    C
292    C
293    C
294    C
295    C
296    C
297    C
298    C
299    C
300    C
301    C
302    C
303    C
304    C
305    C
306    C
307    C
308    C
309    C
310    C
311    C
312    C
313    C
314    C
315    C
316    C
317    C
318    C
319    C
320    C
321    C
322    C
323    C
324    C
325    C
326    C
327    C
328    C
329    C
330    C
331    C
332    C
333    C
334    C
335    C
336    C
337    C
338    C
339    C
340    C
341    C
342    C
343    C
344    C
345    C
346    C
347    C
348    C
349    C
350    C
351    C
352    C
353    C
354    C
355    C
356    C
357    C
358    C
359    C
360    C
361    C
362    C
363    C
364    C
365    C
366    C
367    C
368    C
369    C
370    C
371    C
372    C
373    C
374    C
375    C
376    C
377    C
378    C
379    C
380    C
381    C
382    C
383    C
384    C
385    C
386    C
387    C
388    C
389    C
390    C
391    C
392    C
393    C
394    C
395    C
396    C
397    C
398    C
399    C
400    C
401    C
402    C
403    C
404    C
405    C
406    C
407    C
408    C
409    C
410    C
411    C
412    C
413    C
414    C
415    C
416    C
417    C
418    C
419    C
420    C
421    C
422    C
423    C
424    C
425    C
426    C
427    C
428    C
429    C
430    C
431    C
432    C
433    C
434    C
435    C
436    C
437    C
438    C
439    C
440    C
441    C
442    C
443    C
444    C
445    C
446    C
447    C
448    C
449    C
450    C
451    C
452    C
453    C
454    C
455    C
456    C
457    C
458    C
459    C
460    C
461    C
462    C
463    C
464    C
465    C
466    C
467    C
468    C
469    C
470    C
471    C
472    C
473    C
474    C
475    C
476    C
477    C
478    C
479    C
480    C
481    C
482    C
483    C
484    C
485    C
486    C
487    C
488    C
489    C
490    C
491    C
492    C
493    C
494    C
495    C
496    C
497    C
498    C
499    C
500    C
501    C
502    C
503    C
504    C
505    C
506    C
507    C
508    C
509    C
510    C
511    C
512    C
513    C
514    C
515    C
516    C
517    C
518    C
519    C
520    C
521    C
522    C
523    C
524    C
525    C
526    C
527    C
528    C
529    C
530    C
531    C
532    C
533    C
534    C
535    C
536    C
537    C
538    C
539    C
540    C
541    C
542    C
543    C
544    C
545    C
546    C
547    C
548    C
549    C
550    C
551    C
552    C
553    C
554    C
555    C
556    C
557    C
558    C
559    C
560    C
561    C
562    C
563    C
564    C
565    C
566    C
567    C
568    C
569    C
570    C
571    C
572    C
573    C
574    C
575    C
576    C
577    C
578    C
579    C
580    C
581    C
582    C
583    C
584    C
585    C
586    C
587    C
588    C
589    C
590    C
591    C
592    C
593    C
594    C
595    C
596    C
597    C
598    C
599    C
600    C
601    C
602    C
603    C
604    C
605    C
606    C
607    C
608    C
609    C
610    C
611    C
612    C
613    C
614    C
615    C
616    C
617    C
618    C
619    C
620    C
621    C
622    C
623    C
624    C
625    C
626    C
627    C
628    C
629    C
630    C
631    C
632    C
633    C
634    C
635    C
636    C
637    C
638    C
639    C
640    C
641    C
642    C
643    C
644    C
645    C
646    C
647    C
648    C
649    C
650    C
651    C
652    C
653    C
654    C
655    C
656    C
657    C
658    C
659    C
660    C
661    C
662    C
663    C
664    C
665    C
666    C
667    C
668    C
669    C
670    C
671    C
672    C
673    C
674    C
675    C
676    C
677    C
678    C
679    C
680    C
681    C
682    C
683    C
684    C
685    C
686    C
687    C
688    C
689    C
690    C
691    C
692    C
693    C
694    C
695    C
696    C
697    C
698    C
699    C
700    C
701    C
702    C
703    C
704    C
705    C
706    C
707    C
708    C
709    C
710    C
711    C
712    C
713    C
714    C
715    C
716    C
717    C
718    C
719    C
720    C
721    C
722    C
723    C
724    C
725    C
726    C
727    C
728    C
729    C
730    C
731    C
732    C
733    C
734    C
735    C
736    C
737    C
738    C
739    C
740    C
741    C
742    C
743    C
744    C
745    C
746    C
747    C
748    C
749    C
750    C
751    C
752    C
753    C
754    C
755    C
756    C
757    C
758    C
759    C
760    C
761    C
762    C
763    C
764    C
765    C
766    C
767    C
768    C
769    C
770    C
771    C
772    C
773    C
774    C
775    C
776    C
777    C
778    C
779    C
780    C
781    C
782    C
783    C
784    C
785    C
786    C
787    C
788    C
789    C
790    C
791    C
792    C
793    C
794    C
795    C
796    C
797    C
798    C
799    C
800    C
801    C
802    C
803    C
804    C
805    C
806    C
807    C
808    C
809    C
810    C
811    C
812    C
813    C
814    C
815    C
816    C
817    C
818    C
819    C
820    C
821    C
822    C
823    C
824    C
825    C
826    C
827    C
828    C
829    C
830    C
831    C
832    C
833    C
834    C
835    C
836    C
837    C
838    C
839    C
840    C
841    C
842    C
843    C
844    C
845    C
846    C
847    C
848    C
849    C
850    C
851    C
852    C
853    C
854    C
855    C
856    C
857    C
858    C
859    C
860    C
861    C
862    C
863    C
864    C
865    C
866    C
867    C
868    C
869    C
870    C
871    C
872    C
873    C
874    C
875    C
876    C
877    C
878    C
879    C
880    C
881    C
882    C
883    C
884    C
885    C
886    C
887    C
888    C
889    C
890    C
891    C
892    C
893    C
894    C
895    C
896    C
897    C
898    C
899    C
900    C
901    C
902    C
903    C
904    C
905    C
906    C
907    C
908    C
909    C
910    C
911    C
912    C
913    C
914    C
915    C
916    C
917    C
918    C
919    C
920    C
921    C
922    C
923    C
924    C
925    C
926    C
927    C
928    C
929    C
930    C
931    C
932    C
933    C
934    C
935    C
936    C
937    C
938    C
939    C
940    C
941    C
942    C
943    C
944    C
945    C
946    C
947    C
948    C
949    C
950    C
951    C
952    C
953    C
954    C
955    C
956    C
957    C
958    C
959    C
960    C
961    C
962    C
963    C
964    C
965    C
966    C
967    C
968    C
969    C
970    C
971    C
972    C
973    C
974    C
975    C
976    C
977    C
978    C
979    C
980    C
981    C
982    C
983    C
984    C
985    C
986    C
987    C
988    C
989    C
990    C
991    C
992    C
993    C
994    C
995    C
996    C
997    C
998    C
999    C
1000   C

```

SUBROUTINE SIMLAT 74/74 OPT=1 FTM 4.8\*518 10/06/80 09.37.33

```

1      C
      C SUBROUTINE SIMLAT
5      C THIS SUBROUTINE IS A SIMULATION PROCEDURE FOR THE PARAMETERS
      C OF THE TVA DOUBLE TRIANGLE MODEL
      C
10     REAL KT1,KT2,KUP,IMP,LOSS,KT23,KUR
      COMMON RUNOFF(800),HYDRO(800),RNOFF(500),RAIN(500),STAGE(500)
      > AREA(664),PHI,DT,U,TL,T2,T3,UP,UR,REL,KT1,KT2,KUP,RN,ITOTAL,
      > ICRASH,IDMAX,NPRF,UYHYDRO(400),NPRO,CNOPT,NBIG,TL,KT23
      > TIME(500),TFLOW(500),TFLOWI(500),SFLOW(500),BSFLOW(500)
      > DUMX(4),DUMY(4),BIGX,OBPEAK,PRPEAK,TPOB,TPPR,ISIM
      > IPLOT,IUNIT,NPRF1,NPRF2,AREA,KUR
      > ITITLE(20),SQM1,SHAPE,SCADD,SINU,CNA,SS,IMP,TLF
      < ILOAD,DLOAD
      C ICRASH IS A CONTROL PARAMETER TO SIGNIFY THAT THE DATA IS INCOMPATABLE
      C WITH THE MODEL BEING USED
      C ICRASH = 0
      C CALCULATE TL
      C TL = U/REL * RN
      C CALCULATE UP,T1,T2
      C UP = K1 * TL
      C T1 = K1 * TL
      C T2 = K2 * UP
      C CALL ADJUST(T1,DT)
      C CALL ADJUST(T2,DT)
      C IF (T2 LE T1) T2 = T1 + DT
      C CALCULATE UR AND T3
      C UR = KUR / TL
      C T3 = T1 + (T2 - T2 * UP) / UR
      C LIMIT T3 TO A REASONABLE VALUE
      C T1 = 15.0 * TL
      C IF (T3 LT T1) T3 = T1
      C T3 = T1
      C CALL ADJUST(T3,DT)
      C IF (T3 LE T2) T3 = T2 + DT
      C AREA = (0.5 * T1 * UP) * (0.5 * (UP * UR * (T2 - T1)) + (0.5 * UR * (T3 - T2)))
      C WRITE(6,360) REL,U,RN,TL,UP,UR,T1,T2,T3,AREA
      C360  FORMAT(6X,"REL",9X,"U",9X,"RN",9X,"TL",8X,"UP",8X,"UR",8X,"T1",8X,"
      > T2",8X,"T3",7X,"AREA"/10F10.3/)
      C UP = (1.0 / AREA) * UP
      C UR = (1.0 / AREA) * UR
      C AREA = (0.5 * T1 * UP) * (0.5 * (UP * UR * (T2 - T1)) + (0.5 * UR * (T3 - T2)))
      C WRITE(6,395)
      C395  FORMAT(10X,"ADJUSTED HYDROGRAPH PARAMETERS"/)
      C WRITE(6,400) UP,UR,T1,T2,T3,AREA
      C400  FORMAT(6X,"UP",8X,"UR",8X,"T1",8X,"T2",8X,"T3",6X,"AREA"/6F10.3///)
      > /
      C RETURN
      C430  END

```

AFRUM 475  
AFRUM 476  
AFRUM 477  
AFRUM 478  
AFRUM 479  
AFRUM 480  
AFRUM 481  
AFRUM 482  
AFRUM 483  
AFRUM 484  
AFRUM 485  
AFRUM 486  
AFRUM 487  
AFRUM 488  
AFRUM 489  
AFRUM 490  
AFRUM 491  
AFRUM 492  
AFRUM 493  
AFRUM 494  
AFRUM 495  
AFRUM 496  
AFRUM 497  
AFRUM 498  
AFRUM 499  
AFRUM 500  
AFRUM 501  
AFRUM 502  
AFRUM 503  
AFRUM 504  
AFRUM 505  
AFRUM 506  
AFRUM 507  
AFRUM 508  
AFRUM 509  
AFRUM 510  
AFRUM 511  
AFRUM 512  
AFRUM 513  
AFRUM 514  
AFRUM 515  
AFRUM 516  
AFRUM 517  
AFRUM 518  
AFRUM 519  
AFRUM 520  
AFRUM 521  
AFRUM 522  
AFRUM 523  
AFRUM 524  
AFRUM 525  
AFRUM 526  
AFRUM 527

SUBROUTINE ADJUST	74/74	OPT=1	FTN 4.8*518	10/06/80	09.37.33
-------------------	-------	-------	-------------	----------	----------

```

1      C
      C SUBROUTINE ADJUST(T,DT)
5      C THIS SUBROUTINE ADJUSTS T1,T2,T3 TO THE NEAREST MULTIPLE OF DT
      C
10     FDELTA=DT
      DELTA=100.0*DT
      N=1
      ADT=N*DELTA
      IF (ADT .GE. T) GO TO 20
      N=N+1
      GO TO 10
15     IF (DELTA .GT. FDELTA) GO TO 30
      GO TO 50
30     DELTA=DELTA/10.0
      N=(N-1)/10
      GO TO 10
20     ADT=ADT - (FDELTA/2.0)
      IF (ADT .GT. T) GO TO 60
      GO TO 70
25     T=DELTA*(N-1)
      RETURN
      END

```

```

AFRUM 528
AFRUM 529
AFRUM 530
AFRUM 531
AFRUM 532
AFRUM 533
AFRUM 534
AFRUM 535
AFRUM 536
AFRUM 537
AFRUM 538
AFRUM 539
AFRUM 540
AFRUM 541
AFRUM 542
AFRUM 543
AFRUM 544
AFRUM 545
AFRUM 546
AFRUM 547
AFRUM 548
AFRUM 549
AFRUM 550
AFRUM 551
AFRUM 552
AFRUM 553

```

SUBROUTINE CONVOL	74774	OPT=1	FTN 4.8+518	10/06/80	09.37.33
1	C				AFRUM 5545
	C				AFRUM 5546
	C				AFRUM 5547
5	C				AFRUM 5548
	C				AFRUM 5549
	C				AFRUM 5550
	C				AFRUM 5551
10	C				AFRUM 5552
	C				AFRUM 5553
	C				AFRUM 5554
	C				AFRUM 5555
	C				AFRUM 5556
15	C				AFRUM 5557
	C				AFRUM 5558
	C				AFRUM 5559
	C				AFRUM 5560
	C				AFRUM 5561
	C				AFRUM 5562
	C				AFRUM 5563
	C				AFRUM 5564
	C				AFRUM 5565
	C				AFRUM 5566
	C				AFRUM 5567
	C				AFRUM 5568
	C				AFRUM 5569
	C				AFRUM 5570
	C				AFRUM 5571
	C				AFRUM 5572
	C				AFRUM 5573
	C				AFRUM 5574
	C				AFRUM 5575
	C				AFRUM 5576
	C				AFRUM 5577
	C				AFRUM 5578
	C				AFRUM 5579
	C				AFRUM 5580
	C				AFRUM 5581
	C				AFRUM 5582
	C				AFRUM 5583
	C				AFRUM 5584
	C				AFRUM 5585
	C				AFRUM 5586
	C				AFRUM 5587
	C				AFRUM 5588
	C				AFRUM 5589
	C				AFRUM 5590
	C				AFRUM 5591
	C				AFRUM 5592
	C				AFRUM 5593
	C				AFRUM 5594
	C				AFRUM 5595
	C				AFRUM 5596
	C				AFRUM 5597
	C				AFRUM 5598
	C				AFRUM 5599
	C				AFRUM 5600
	C				AFRUM 5601
	C				AFRUM 5602
	C				AFRUM 5603
	C				AFRUM 5604
	C				AFRUM 5605
	C				AFRUM 5606
	C				AFRUM 5607
	C				AFRUM 5608
	C				AFRUM 5609
	C				AFRUM 5610
	C				AFRUM 5611
	C				AFRUM 5612
	C				AFRUM 5613
	C				AFRUM 5614
	C				AFRUM 5615
	C				AFRUM 5616
	C				AFRUM 5617
	C				AFRUM 5618
	C				AFRUM 5619
	C				AFRUM 5620
	C				AFRUM 5621
	C				AFRUM 5622
	C				AFRUM 5623
	C				AFRUM 5624
	C				AFRUM 5625
	C				AFRUM 5626
	C				AFRUM 5627
	C				AFRUM 5628
	C				AFRUM 5629
	C				AFRUM 5630
	C				AFRUM 5631
	C				AFRUM 5632
	C				AFRUM 5633
	C				AFRUM 5634
	C				AFRUM 5635
	C				AFRUM 5636
	C				AFRUM 5637
	C				AFRUM 5638
	C				AFRUM 5639
	C				AFRUM 5640
	C				AFRUM 5641
	C				AFRUM 5642
	C				AFRUM 5643
	C				AFRUM 5644</

```

65      170      CONTINUE
        185      HYDRO(N3)=0.0
        C      WRITE(6,185)
        C      FORMAT(////)
70      192      CONVOLUTE HYDROGRAPH WITH EXCESS RAINFALL
        193      ITOTAL=N3+NPRF-1
        194      IF (ITOTAL.LT. 800) GO TO 193
        195      WRITE(6,192)
        196      FORMAT(5X,"STORAGE SPACE EXCEEDED. KILL JOB")
        197      ICRASH=1
        198      GO TO 451
        199      DO 194 I=1,N3
        200      UHYDRO(I)=HYDRO(I)
        201      CONTINUE
        202      DO 195 I=1,IDMAX
        203      HYDRO(I)=0.0
        204      CONTINUE
        205      DO 196 I=1,IDMAX
        206      RUNOFF(I)=0.0
        207      CONTINUE
        208      DO 197 I=1,N3
        209      HYDRO(I)=UHYDRO(I)*PE(I)
        210      CONTINUE
        211      DO 300 J=2,NPRF
        212      JMIN=J-1
        213      JMAX=JMIN+N3
        214      DO 209 JJ=1,JMIN
        215      RUNOFF(JJ)=0.0
        216      CONTINUE
        217      K=J
        218      DO 210 JJ=K,JMAX
        219      RUNOFF(JJ)=UHYDRO(JJ-JMIN)*PE(K)
        220      CONTINUE
        221      DO 220 JJ=1,JMAX
        222      UHYDRO(JJ)=HYDRO(JJ)+RUNOFF(JJ)
        223      CONTINUE
        224      DO 221 JJ=1,JMAX
        225      CONTINUE
        226      NBIG=ITOTAL
        227      IF (NPRO.GT. NBIG) NBIG=NPRO
        228      BIGX=0.0
        229      OBPEAK=0.0
        230      PRPEAK=0.0
        231      TPOR=0.0
        232      TIME(I)=0.0
        233      HYDRO(I)=0.0
        234      RUNOFF(I)=0.0
        235      DO 340 I=2,NBIG
        236      TIME(I)=TIME(I-1)+DT
        237      CONTINUE
        238      IT1=ITOTAL+1
        239      DO 350 I=IT1,IDMAX
        240      HYDRO(I)=0.0
        241      CONTINUE
        242      NPRO=NPRO+1
        243      DO 360 I=NPRO1,IDMAX
        244      RUNOFF(I)=0.0
        245      CONTINUE
        246      IF (UNIT.EQ.0) GO TO 368
        247      CONVRT=(SQRT(40.*3560.))/(3600.*12.)
        248      DO 365 I=1,NBIG
        249      HYDRO(I)=HYDRO(I)*CONVRT
        250      RUNOFF(I)=RUNOFF(I)*CONVRT
        251      CONTINUE
        252      DO 410 I=1,NBIG
        253      UHYDRO(I)=HYDRO(I)
        254      GO TO 380
        255      PRPEAK=HYDRO(I)
        256      370

```



```

135      TPR=TIME(I)
136      CONTINUE
137      GO TO 385
140      OBPEAK=ROFF(I)
141      TPOB=TIME(I)
142      CONTINUE
143      IF (I1STM.EQ.1) OBPEAK=0.0
144      IF (I1STM.EQ.1) TPOB=0.0
145      IF (OBPEAK.GT.8IGY) 8IGY=OBPEAK
146      GO TO 430
150      CONTINUE
151      WRITE(6,411) TPOB,TPPR
152      FORMAT(4X,"OBSERVED",10X,"PREDICTED"/
153      >2X,"TIME TO PEAK",5X,"TIME TO PEAK"/
154      >4X,"HOURS",10X,"HOURS"/
155      >F10.3,F10.3)
156      IF (IUNIT.EQ.1) GO TO 420
157      WRITE(6,412) OBPEAK,PRPEAK
158      FORMAT(12X,"OBSERVED PEAK",5X,"PREDICTED PEAK"/
159      >5X,"(IN/HR)",11X,"(IN/HR)"/
160      >F11.5,F11.5)
161      GO TO 4519
162      WRITE(6,425) OBPEAK,PRPEAK
163      FORMAT(12X,"OBSERVED PEAK",5X,"PREDICTED PEAK"/
164      >6X,"(CFS)",12X,"(CFS)"/
165      >F11.5,F11.5)
166      GO TO 4519
167      8IGX=1ML/NBIG
168      DUMX(1)=0.0
169      DUMX(2)=8IGX
170      DUMX(3)=8IGY
171      DUMX(4)=8IGY
172      NPROF=NBIG+2
173      ARATE=MIN/HR
174      IF (IUNIT.NE.0) ARATE="(CFS)"
175      BRATE=7HLBS/HR
176      IF (IUNIT.NE.0) BRATE=7HLBS/SEC
177      WRITE(6,4300)
178      FORMAT(1M,18X,"TABLE I. HYDROGRAPH OUTPUT",///)
179      IF (ILOAD.NE.0) WRITE(6,434)
180      IF (ILOAD.NE.0) WRITE(6,434)
181      WRITE(6,436)
182      FORMAT(7X,"OBSERVED",6X,"PREDICTED")
183      IF (ILOAD.NE.0) WRITE(6,437)
184      IF (ILOAD.NE.0) WRITE(6,437)
185      WRITE(6,438)
186      FORMAT(8X,"FLOW OUT OF",3X,"FLOW OUT OF")
187      IF (ILOAD.NE.0) WRITE(6,439)
188      IF (ILOAD.NE.0) WRITE(6,439)
189      WRITE(6,4391)
190      FORMAT(6X,"WATERSHED",5X,"WATERSHED",8X,"TIME")
191      IF (ILOAD.NE.0) WRITE(6,4392)
192      IF (ILOAD.NE.0) WRITE(6,4392)
193      IF (ILOAD.NE.0) WRITE(6,4393)
194      IF (ILOAD.NE.0) WRITE(6,4393)
195      IF (ILOAD.NE.0) WRITE(6,4394)
196      IF (ILOAD.NE.0) WRITE(6,4394)
197      IF (ILOAD.NE.0) WRITE(6,4395)
198      IF (ILOAD.NE.0) WRITE(6,4395)
199      IF (ILOAD.NE.0) WRITE(6,4396)
200      IF (ILOAD.NE.0) WRITE(6,4396)
201      IF (ILOAD.NE.0) WRITE(6,4397)
202      IF (ILOAD.NE.0) WRITE(6,4397)
203      IF (ILOAD.NE.0) WRITE(6,4398)
204      IF (ILOAD.NE.0) WRITE(6,4398)
205      IF (ILOAD.NE.0) WRITE(6,4399)
206      IF (ILOAD.NE.0) WRITE(6,4399)
207      IF (ILOAD.NE.0) WRITE(6,4400)
208      IF (ILOAD.NE.0) WRITE(6,4400)
209      IF (ILOAD.NE.0) WRITE(6,4401)
210      IF (ILOAD.NE.0) WRITE(6,4401)
211      IF (ILOAD.NE.0) WRITE(6,4402)
212      IF (ILOAD.NE.0) WRITE(6,4402)
213      IF (ILOAD.NE.0) WRITE(6,4403)
214      IF (ILOAD.NE.0) WRITE(6,4403)
215      IF (ILOAD.NE.0) WRITE(6,4404)
216      IF (ILOAD.NE.0) WRITE(6,4404)
217      IF (ILOAD.NE.0) WRITE(6,4405)
218      IF (ILOAD.NE.0) WRITE(6,4405)
219      IF (ILOAD.NE.0) WRITE(6,4406)
220      IF (ILOAD.NE.0) WRITE(6,4406)
221      IF (ILOAD.NE.0) WRITE(6,4407)
222      IF (ILOAD.NE.0) WRITE(6,4407)
223      IF (ILOAD.NE.0) WRITE(6,4408)
224      IF (ILOAD.NE.0) WRITE(6,4408)
225      IF (ILOAD.NE.0) WRITE(6,4409)
226      IF (ILOAD.NE.0) WRITE(6,4409)
227      IF (ILOAD.NE.0) WRITE(6,4410)
228      IF (ILOAD.NE.0) WRITE(6,4410)
229      IF (ILOAD.NE.0) WRITE(6,4411)
230      IF (ILOAD.NE.0) WRITE(6,4411)
231      IF (ILOAD.NE.0) WRITE(6,4412)
232      IF (ILOAD.NE.0) WRITE(6,4412)
233      IF (ILOAD.NE.0) WRITE(6,4413)
234      IF (ILOAD.NE.0) WRITE(6,4413)
235      IF (ILOAD.NE.0) WRITE(6,4414)
236      IF (ILOAD.NE.0) WRITE(6,4414)
237      IF (ILOAD.NE.0) WRITE(6,4415)
238      IF (ILOAD.NE.0) WRITE(6,4415)
239      IF (ILOAD.NE.0) WRITE(6,4416)
240      IF (ILOAD.NE.0) WRITE(6,4416)
241      IF (ILOAD.NE.0) WRITE(6,4417)
242      IF (ILOAD.NE.0) WRITE(6,4417)
243      IF (ILOAD.NE.0) WRITE(6,4418)
244      IF (ILOAD.NE.0) WRITE(6,4418)
245      IF (ILOAD.NE.0) WRITE(6,4419)
246      IF (ILOAD.NE.0) WRITE(6,4419)
247      IF (ILOAD.NE.0) WRITE(6,4420)
248      IF (ILOAD.NE.0) WRITE(6,4420)
249      IF (ILOAD.NE.0) WRITE(6,4421)
250      IF (ILOAD.NE.0) WRITE(6,4421)
251      IF (ILOAD.NE.0) WRITE(6,4422)
252      IF (ILOAD.NE.0) WRITE(6,4422)
253      IF (ILOAD.NE.0) WRITE(6,4423)
254      IF (ILOAD.NE.0) WRITE(6,4423)
255      IF (ILOAD.NE.0) WRITE(6,4424)
256      IF (ILOAD.NE.0) WRITE(6,4424)
257      IF (ILOAD.NE.0) WRITE(6,4425)
258      IF (ILOAD.NE.0) WRITE(6,4425)
259      IF (ILOAD.NE.0) WRITE(6,4426)
260      IF (ILOAD.NE.0) WRITE(6,4426)
261      IF (ILOAD.NE.0) WRITE(6,4427)
262      IF (ILOAD.NE.0) WRITE(6,4427)
263      IF (ILOAD.NE.0) WRITE(6,4428)
264      IF (ILOAD.NE.0) WRITE(6,4428)
265      IF (ILOAD.NE.0) WRITE(6,4429)
266      IF (ILOAD.NE.0) WRITE(6,4429)
267      IF (ILOAD.NE.0) WRITE(6,4430)
268      IF (ILOAD.NE.0) WRITE(6,4430)
269      IF (ILOAD.NE.0) WRITE(6,4431)
270      IF (ILOAD.NE.0) WRITE(6,4431)
271      IF (ILOAD.NE.0) WRITE(6,4432)
272      IF (ILOAD.NE.0) WRITE(6,4432)
273      IF (ILOAD.NE.0) WRITE(6,4433)
274      IF (ILOAD.NE.0) WRITE(6,4433)
275      IF (ILOAD.NE.0) WRITE(6,4434)
276      IF (ILOAD.NE.0) WRITE(6,4434)
277      IF (ILOAD.NE.0) WRITE(6,4435)
278      IF (ILOAD.NE.0) WRITE(6,4435)
279      IF (ILOAD.NE.0) WRITE(6,4436)
280      IF (ILOAD.NE.0) WRITE(6,4436)
281      IF (ILOAD.NE.0) WRITE(6,4437)
282      IF (ILOAD.NE.0) WRITE(6,4437)
283      IF (ILOAD.NE.0) WRITE(6,4438)
284      IF (ILOAD.NE.0) WRITE(6,4438)
285      IF (ILOAD.NE.0) WRITE(6,4439)
286      IF (ILOAD.NE.0) WRITE(6,4439)
287      IF (ILOAD.NE.0) WRITE(6,4440)
288      IF (ILOAD.NE.0) WRITE(6,4440)
289      IF (ILOAD.NE.0) WRITE(6,4441)
290      IF (ILOAD.NE.0) WRITE(6,4441)
291      IF (ILOAD.NE.0) WRITE(6,4442)
292      IF (ILOAD.NE.0) WRITE(6,4442)
293      IF (ILOAD.NE.0) WRITE(6,4443)
294      IF (ILOAD.NE.0) WRITE(6,4443)
295      IF (ILOAD.NE.0) WRITE(6,4444)
296      IF (ILOAD.NE.0) WRITE(6,4444)
297      IF (ILOAD.NE.0) WRITE(6,4445)
298      IF (ILOAD.NE.0) WRITE(6,4445)
299      IF (ILOAD.NE.0) WRITE(6,4446)
300      IF (ILOAD.NE.0) WRITE(6,4446)
301      IF (ILOAD.NE.0) WRITE(6,4447)
302      IF (ILOAD.NE.0) WRITE(6,4447)
303      IF (ILOAD.NE.0) WRITE(6,4448)
304      IF (ILOAD.NE.0) WRITE(6,4448)
305      IF (ILOAD.NE.0) WRITE(6,4449)
306      IF (ILOAD.NE.0) WRITE(6,4449)
307      IF (ILOAD.NE.0) WRITE(6,4450)
308      IF (ILOAD.NE.0) WRITE(6,4450)
309      IF (ILOAD.NE.0) WRITE(6,4451)
310      IF (ILOAD.NE.0) WRITE(6,4451)
311      IF (ILOAD.NE.0) WRITE(6,4452)
312      IF (ILOAD.NE.0) WRITE(6,4452)
313      IF (ILOAD.NE.0) WRITE(6,4453)
314      IF (ILOAD.NE.0) WRITE(6,4453)
315      IF (ILOAD.NE.0) WRITE(6,4454)
316      IF (ILOAD.NE.0) WRITE(6,4454)
317      IF (ILOAD.NE.0) WRITE(6,4455)
318      IF (ILOAD.NE.0) WRITE(6,4455)
319      IF (ILOAD.NE.0) WRITE(6,4456)
320      IF (ILOAD.NE.0) WRITE(6,4456)
321      IF (ILOAD.NE.0) WRITE(6,4457)
322      IF (ILOAD.NE.0) WRITE(6,4457)
323      IF (ILOAD.NE.0) WRITE(6,4458)
324      IF (ILOAD.NE.0) WRITE(6,4458)
325      IF (ILOAD.NE.0) WRITE(6,4459)
326      IF (ILOAD.NE.0) WRITE(6,4459)
327      IF (ILOAD.NE.0) WRITE(6,4460)
328      IF (ILOAD.NE.0) WRITE(6,4460)
329      IF (
```

680	AFRUM
681	AFRUM
682	AFRUM
683	AFRUM
684	AFRUM
685	AFRUM
686	AFRUM
687	AFRUM
688	AFRUM
689	AFRUM
690	AFRUM
691	AFRUM
692	AFRUM
693	AFRUM
694	AFRUM
695	AFRUM
696	AFRUM
697	AFRUM
698	AFRUM
699	AFRUM
700	AFRUM
701	AFRUM
702	AFRUM
703	AFRUM
704	AFRUM
705	AFRUM
706	AFRUM
707	AFRUM
708	AFRUM
709	AFRUM
710	AFRUM
711	AFRUM
712	AFRUM
713	AFRUM
714	AFRUM
715	AFRUM
716	AFRUM
717	AFRUM
718	AFRUM
719	AFRUM
720	AFRUM
721	AFRUM
722	AFRUM
723	AFRUM
724	AFRUM
725	AFRUM
726	AFRUM
727	AFRUM
728	AFRUM
729	AFRUM
730	AFRUM
731	AFRUM
732	AFRUM
733	AFRUM
734	AFRUM
735	AFRUM
736	AFRUM
737	AFRUM
738	AFRUM
739	AFRUM
740	AFRUM
741	AFRUM
742	AFRUM
743	AFRUM
744	AFRUM
745	AFRUM
746	AFRUM
747	AFRUM
748	AFRUM
749	AFRUM
750	AFRUM
751	AFRUM
752	AFRUM
753	AFRUM
754	AFRUM
755	AFRUM
756	AFRUM
757	AFRUM

[illegible]

SUBROUTINE BASINA	74/74	OPT=1	FTN 4.8.518	10/06/80	09.37.33
-------------------	-------	-------	-------------	----------	----------

```

1      C
      C
5      C
      C
      SUBROUTINE BASINA(SOMI,PF,PS,BDATE,BASIN,PI)
      DIMENSION BASIN(4)
      WRITE(6,10) BASIN,BDATE,SOMI,PF,PS,PI
10  FORMAT(46X,"THE WATERSHED NAME IS",A10,"/,"
      >36X,"THE DATE OF THE RAINFALL EVENT IS",A8,"/,"
      >36X,"THE WATERSHED SIZE IN SQUARE MILES IS",
      >36X,"THE PERCENT OF THE BASIN WHICH IS FOREST IS: ",
      >36X,"THE PERCENT OF THE BASIN DENUDED IS: ",
      >36X,"THE PERCENT OF THE BASIN WHICH IS IMPERVIOUS IS: PI= ",F8.2//
      RETURN
      END

```

```

AFRUM 1054
AFRUM 1055
AFRUM 1056
AFRUM 1057
AFRUM 1058
AFRUM 1059
AFRUM 1060
AFRUM 1061
AFRUM 1062
AFRUM 1063
AFRUM 1064
AFRUM 1065
AFRUM 1066
AFRUM 1067
AFRUM 1068

```

```

SUBROUTINE ASSUME 74/74 OPT=1 FTN 4.8+518 09.37.33
C
C SUBROUTINE ASSUME (ISIM,IPMT,IUNIT,IPILOT,ICHAR,ILAG,ILOAD)
C
5 IF (ISIM.EQ.1) GO TO 10
WRITE (6,5)
*BY SETTING ISIM = 0 YOU HAVE INDICATED THAT YOU PLAN"/,
*36X,"TO SUPPLY EITHER ACTUAL OR DESIGN RAINFALL AND RUNOFF"/,
*36X,"DATA; THEREFORE, THE SCS CURVE NUMBER, CN, WILL BE DE-"/,
*36X,"TERMINED BY SETTING RUNOFF EQUAL TO PRECIPITATION EXCESS."/,
GO TO 12
10 WRITE (6,15)
15 FORMAT (46X,
*BY SETTING ISIM = 1 YOU HAVE INDICATED THAT YOU PLAN"/,
*36X,"TO SUPPLY ACTUAL OR DESIGN RAINFALL DATA; THEREFORE, AN"/,
*36X,"ESTIMATE OF THE SCS CURVE NUMBER, CN, MUST BE PROVIDED."/)
12 CONTINUE
IPILOT = EQ.1) GO TO 25
IPILOT = EQ.0) GO TO 25
20 *36X,"AND INCHES AS SELECTED BY SETTING IUNIT = 0."/,
GO TO 32
25 WRITE (6,30)
30 FORMAT (46X,"OUTPUT UNITS OF THE SIMULATED HYDROGRAPH ARE HOURS"/,
*36X,"AND CUBIC FEET PER SECOND. CFS, AS SELECTED BY SETTING"/,
*36X,"IUNIT = 1."/)
32 CONTINUE
IPILOT = EQ.1) GO TO 40
IPILOT = EQ.0) GO TO 40
35 FORMAT (46X,"NO PLOT HAS BEEN REQUESTED; IPILOT = 0."/,
GO TO 47
40 WRITE (6,45)
45 FORMAT (46X,"YOU HAVE REQUESTED THAT THE HYDROGRAPH BE PLOTTED"/,
*36X,"BY SETTING IPILOT = 1."/)
47 CONTINUE
IPILOT = EQ.0) GO TO 55
IPILOT = EQ.1) GO TO 55
50 *36X,"THE WATERSHED IS ASSUMED TO BE URBAN WITHOUT"/,
GO TO 100
55 IF (ICHAR.GT.1) GO TO 65
WRITE (6,60)
60 FORMAT (46X,"THE WATERSHED IS ASSUMED TO BE URBAN WITH STORM"/,
*36X,"SEWERS; ICHAR = 1."/)
GO TO 100
65 IF (ICHAR.GT.2) GO TO 75
WRITE (6,70)
70 FORMAT (46X,"THE WATERSHED IS SIMILAR TO A COAL STRIP MINE"/,
*36X,"AREA, OR DENuded FOREST AREA; ICHAR = 2."/)
GO TO 100
75 IF (ICHAR.GT.3) GO TO 85
WRITE (6,80)
80 FORMAT (46X,"THE WATERSHED IS MOSTLY AGRICULTURAL; ICHAR = 3X"/,
GO TO 100
85 IF (ICHAR.GT.4) GO TO 95
WRITE (6,90)
90 *36X,"YOU HAVE SET ICHAR = 4."/)
100 CONTINUE
IPILOT = EQ.0) GO TO 110
IPILOT = EQ.1) GO TO 110
105 FORMAT (46X,"YOU HAVE DECIDED TO SELECT A VALUE FOR LAG"/,
*36X,"MODULUS IN HOURS; ILAG = 0."/)

```

	09.37.33
FURUM	069
FURUM	070
FURUM	071
FURUM	072
FURUM	073
FURUM	074
FURUM	075
FURUM	076
FURUM	077
FURUM	078
FURUM	079
FURUM	080
FURUM	081
FURUM	082
FURUM	083
FURUM	084
FURUM	085
FURUM	086
FURUM	087
FURUM	088
FURUM	089
FURUM	090
FURUM	091
FURUM	092
FURUM	093
FURUM	094
FURUM	095
FURUM	096
FURUM	097
FURUM	098
FURUM	099
FURUM	100
FURUM	101
FURUM	102
FURUM	103
FURUM	104
FURUM	105
FURUM	106
FURUM	107
FURUM	108
FURUM	109
FURUM	110
FURUM	111
FURUM	112
FURUM	113
FURUM	114
FURUM	115
FURUM	116
FURUM	117
FURUM	118
FURUM	119
FURUM	120
FURUM	121
FURUM	122
FURUM	123
FURUM	124
FURUM	125
FURUM	126
FURUM	127
FURUM	128
FURUM	129
FURUM	130
FURUM	131
FURUM	132
FURUM	133
FURUM	134
FURUM	135
FURUM	136
FURUM	137
FURUM	138
FURUM	139
FURUM	140
FURUM	141
FURUM	142
FURUM	143
FURUM	144
FURUM	145
FURUM	146
FURUM	147
FURUM	148
FURUM	149
FURUM	150
FURUM	151
FURUM	152
FURUM	153
FURUM	154
FURUM	155
FURUM	156
FURUM	157
FURUM	158
FURUM	159
FURUM	160
FURUM	161
FURUM	162
FURUM	163
FURUM	164
FURUM	165
FURUM	166
FURUM	167
FURUM	168
FURUM	169
FURUM	170
FURUM	171
FURUM	172
FURUM	173
FURUM	174
FURUM	175
FURUM	176
FURUM	177
FURUM	178
FURUM	179
FURUM	180
FURUM	181
FURUM	182
FURUM	183
FURUM	184
FURUM	185
FURUM	186
FURUM	187
FURUM	188
FURUM	189
FURUM	190
FURUM	191
FURUM	192
FURUM	193
FURUM	194
FURUM	195
FURUM	196
FURUM	197
FURUM	198
FURUM	199
FURUM	200

3/06/80

1  
F" , / ,  
E - " , / ,  
CESS. " , / , / ,  
AN" , / ,  
ED. " , / ,  
HOURS " , / ,  
HOURS " , / ,  
NG " , / ,  
TTED " , / ,  
 , / ,  
RM " , / ,  
" , / ,  
3X " , / ,  
D " , / ,  
 ,

PLAN".,/.,  
AND RUNOF  
WILL BE D  
ATION EX

PLAN".,/.,  
HEREFORE,  
BE PROVID

GRAPH ARE  
".,/.,

GRAPH ARE  
BY SETTI

2.".,/.)

GRAPH BE PLO

WITHOUT"

WITH STO

TRIP MINE

ICHAR =

Y FORESTE

DR LAG".,/.

ICHAR, ILA  
THAT YOU  
AINFALL A  
ER. CN, V  
PRECIPI  
THAT YOU  
DATA: T  
N. MUST  
D HYDROG  
UNIT  $\approx 0$   
D HYDROG  
SELECTED  
IPLOT =  
HYDROGRAP  
BE URBAN  
BE URBAN  
A COAL S  
t = 2.4, 1  
CULTURAL  
BE MOSTL  
A VALUE F

II, PLOT,  
INDICATED  
DESIGN R  
CURVE NUMB  
EQUAL TO  
INDICATED  
TRAINFALL  
NUMBER, C  
SIMULATE  
SETTING I  
SIMULATE  
CFS. AS  
REQUESTED;  
THAT THE  
SUMMED TO  
/)  
SUMMED TO  
SIMILAR TO  
AREA; ICHAR  
STLY AGRI  
SUMMED TO  
SELECT A  
"."/

IPHI,IUN  
YOU HAVE I  
FACTUAL OR  
THE SCS C  
ING RUNOFF  
5  
YOU HAVE I  
DESIGN  
SS CURVE  
5  
IS OF THE  
CTED BY  
5  
IS OF THE  
SECOND,  
0  
S BEEN RE  
REQUESTED  
= 1."./)  
5  
ED IS AS  
AR = 0."  
5  
ED IS AS  
= 1."./)  
5  
ED IS SI  
FOREST AR  
5  
ED IS MO  
ED IS AS  
= 4."./)  
0  
ECIDED TO  
LAG = 0

```

OPT=1
VOLUME (ISIM
GO TO 10
IM = 0 YC
EITHER A
BEFORE: 1
BY SETTING
IM = 1 YC
ACTUAL C
OF THE SC
GO TO 28
INPUT UNIT
S AS SELE
INPUT UNIT
FEET PER
".")
GO TO 4
PLOT HAS
U HAVE RE
G IPLOT =
GO TO 55
E WATERS
E WATERS
GO TO 65
E WATERS
E WATERS
GO TO 79
E WATERS
E WATERS
GO TO 89
E WATERS
E WATERS
GO TO 11
U HAVE DE
U HAVE DE
HOURS:

```

[illegible][illegible]

ROUTINE AS

CC

CC

S

1

1

70

\_\_\_\_\_

```

65      GO TO 130
110      IF (LAG.GT.1) GO TO 120
115      WRITE(6,115)
120      FORMAT(46X,"YOU HAVE ELECTED TO SIMULATE LAG MODULUS IN"/,
125      >36X,"HOURS ASSUMING IT IS A FUNCTION OF THE WATERSHED AREA"/,
130      >36X,"AND PERCENT IMPERVIOUS AREA OF THE WATERSHED" ILAG = 1.,//)
135      GO TO 130
140      WRITE(6,125)
145      FORMAT(46X,"YOU HAVE ELECTED TO SIMULATE LAG MODULUS IN"/,
150      >36X,"HOURS ASSUMING IT IS A FUNCTION OF THE RURAL WATERSHED"/,
155      >36X,"AREA AND THE PERCENT OF THE WATERSHED THAT IS FORESTED"/,
160      >36X,"LAG = 2."//)
165      CONTINUE
170      IF (LOAD.EQ.2) GO TO 140
175      WRITE(6,135)
180      FORMAT(46X,"SEDIMENT LOAD HAS BEEN SIMULATED ASSUMING THE"/,
185      >36X,"WATERSHED IS RURAL OR URBAN WITHOUT MAJOR CONSTRUCTION"/,
190      >36X,"LOAD = 1."//)
195      GO TO 150
200      WRITE(6,145)
205      FORMAT(46X,"SEDIMENT LOAD HAS BEEN SIMULATED ASSUMING THE"/,
210      >36X,"WATERSHED IS A DENUDED FOREST AREA OR A COAL STRIP MINE"/,
215      >36X,"AREA LOAD = 2."///// )
220      CONTINUE
225      WRITE(6,160)
230      FORMAT(46X,"RETURN")
235      END

```

```

AFRUM 1133
AFRUM 1134
AFRUM 1135
AFRUM 1136
AFRUM 1137
AFRUM 1138
AFRUM 1139
AFRUM 1140
AFRUM 1141
AFRUM 1142
AFRUM 1143
AFRUM 1144
AFRUM 1145
AFRUM 1146
AFRUM 1147
AFRUM 1148
AFRUM 1149
AFRUM 1150
AFRUM 1151
AFRUM 1152
AFRUM 1153
AFRUM 1154
AFRUM 1155
AFRUM 1156
AFRUM 1157
AFRUM 1158
AFRUM 1159
AFRUM 1160

```



SUBROUTINE HYPLOT 74/74 OPT=1 FTM 4.8\*518 10/06/80 09.37.33

```

1      C
2      C
3      C
4      C
5      C
6      C
7      C
8      C
9      C
10     C
11     C
12     C
13     C
14     C
15     C
16     C
17     C
18     C
19     C
20     C
21     C
22     C
23     C
24     C
25     C
26     C
27     C
28     C
29     C
30     C
31     C
32     C
33     C
34     C
35     C
36     C
37     C
38     C
39     C
40     C
41     C
42     C
43     C
44     C
45     C
46     C
47     C
48     C
49     C
50     C
51     C
52     C
53     C
54     C
55     C
56     C
57     C
58     C
59     C
60     C
61     C
62     C
63     C
64     C
65     C
66     C
67     C
68     C
69     C
70     C
71     C
72     C
73     C
74     C
75     C
76     C
77     C
78     C
79     C
80     C
81     C
82     C
83     C
84     C
85     C
86     C
87     C
88     C
89     C
90     C
91     C
92     C
93     C
94     C
95     C
96     C
97     C
98     C
99     C
100    C
101    C
102    C
103    C
104    C
105    C
106    C
107    C
108    C
109    C
110    C
111    C
112    C
113    C
114    C
115    C
116    C
117    C
118    C
119    C
120    C
121    C
122    C
123    C
124    C
125    C
126    C
127    C
128    C
129    C
130    C
131    C
132    C
133    C
134    C
135    C
136    C
137    C
138    C
139    C
140    C
141    C
142    C
143    C
144    C
145    C
146    C
147    C
148    C
149    C
150    C
151    C
152    C
153    C
154    C
155    C
156    C
157    C
158    C
159    C
160    C
161    C
162    C
163    C
164    C
165    C
166    C
167    C
168    C
169    C
170    C
171    C
172    C
173    C
174    C
175    C
176    C
177    C
178    C
179    C
180    C
181    C
182    C
183    C
184    C
185    C
186    C
187    C
188    C
189    C
190    C
191    C
192    C
193    C
194    C
195    C
196    C
197    C
198    C
199    C
200    C
201    C
202    C
203    C
204    C
205    C
206    C
207    C
208    C
209    C
210    C
211    C
212    C
213    C
214    C
215    C
216    C
217    C
218    C
219    C
220    C
221    C
222    C
223    C
224    C
225    C
226    C
227    C
228    C
229    C
230    C
231    C
232    C
233    C
234    C
235    C
236    C
237    C
238    C
239    C
240    C
241    C
242    C
243    C
244    C
245    C
246    C
247    C
248    C
249    C
250    C
251    C
252    C
253    C
254    C
255    C
256    C
257    C
258    C
259    C
260    C
261    C
262    C
263    C
264    C
265    C
266    C
267    C
268    C
269    C
270    C
271    C
272    C
273    C
274    C
275    C
276    C
277    C
278    C
279    C
280    C
281    C
282    C
283    C
284    C
285    C
286    C
287    C
288    C
289    C
290    C
291    C
292    C
293    C
294    C
295    C
296    C
297    C
298    C
299    C
300    C
301    C
302    C
303    C
304    C
305    C
306    C
307    C
308    C
309    C
310    C
311    C
312    C
313    C
314    C
315    C
316    C
317    C
318    C
319    C
320    C
321    C
322    C
323    C
324    C
325    C
326    C
327    C
328    C
329    C
330    C
331    C
332    C
333    C
334    C
335    C
336    C
337    C
338    C
339    C
340    C
341    C
342    C
343    C
344    C
345    C
346    C
347    C
348    C
349    C
350    C
351    C
352    C
353    C
354    C
355    C
356    C
357    C
358    C
359    C
360    C
361    C
362    C
363    C
364    C
365    C
366    C
367    C
368    C
369    C
370    C
371    C
372    C
373    C
374    C
375    C
376    C
377    C
378    C
379    C
380    C
381    C
382    C
383    C
384    C
385    C
386    C
387    C
388    C
389    C
390    C
391    C
392    C
393    C
394    C
395    C
396    C
397    C
398    C
399    C
400    C
401    C
402    C
403    C
404    C
405    C
406    C
407    C
408    C
409    C
410    C
411    C
412    C
413    C
414    C
415    C
416    C
417    C
418    C
419    C
420    C
421    C
422    C
423    C
424    C
425    C
426    C
427    C
428    C
429    C
430    C
431    C
432    C
433    C
434    C
435    C
436    C
437    C
438    C
439    C
440    C
441    C
442    C
443    C
444    C
445    C
446    C
447    C
448    C
449    C
450    C
451    C
452    C
453    C
454    C
455    C
456    C
457    C
458    C
459    C
460    C
461    C
462    C
463    C
464    C
465    C
466    C
467    C
468    C
469    C
470    C
471    C
472    C
473    C
474    C
475    C
476    C
477    C
478    C
479    C
480    C
481    C
482    C
483    C
484    C
485    C
486    C
487    C
488    C
489    C
490    C
491    C
492    C
493    C
494    C
495    C
496    C
497    C
498    C
499    C
500    C
501    C
502    C
503    C
504    C
505    C
506    C
507    C
508    C
509    C
510    C
511    C
512    C
513    C
514    C
515    C
516    C
517    C
518    C
519    C
520    C
521    C
522    C
523    C
524    C
525    C
526    C
527    C
528    C
529    C
530    C
531    C
532    C
533    C
534    C
535    C
536    C
537    C
538    C
539    C
540    C
541    C
542    C
543    C
544    C
545    C
546    C
547    C
548    C
549    C
550    C
551    C
552    C
553    C
554    C
555    C
556    C
557    C
558    C
559    C
560    C
561    C
562    C
563    C
564    C
565    C
566    C
567    C
568    C
569    C
570    C
571    C
572    C
573    C
574    C
575    C
576    C
577    C
578    C
579    C
580    C
581    C
582    C
583    C
584    C
585    C
586    C
587    C
588    C
589    C
590    C
591    C
592    C
593    C
594    C
595    C
596    C
597    C
598    C
599    C
600    C
601    C
602    C
603    C
604    C
605    C
606    C
607    C
608    C
609    C
610    C
611    C
612    C
613    C
614    C
615    C
616    C
617    C
618    C
619    C
620    C
621    C
622    C
623    C
624    C
625    C
626    C
627    C
628    C
629    C
630    C
631    C
632    C
633    C
634    C
635    C
636    C
637    C
638    C
639    C
640    C
641    C
642    C
643    C
644    C
645    C
646    C
647    C
648    C
649    C
650    C
651    C
652    C
653    C
654    C
655    C
656    C
657    C
658    C
659    C
660    C
661    C
662    C
663    C
664    C
665    C
666    C
667    C
668    C
669    C
670    C
671    C
672    C
673    C
674    C
675    C
676    C
677    C
678    C
679    C
680    C
681    C
682    C
683    C
684    C
685    C
686    C
687    C
688    C
689    C
690    C
691    C
692    C
693    C
694    C
695    C
696    C
697    C
698    C
699    C
700    C
701    C
702    C
703    C
704    C
705    C
706    C
707    C
708    C
709    C
710    C
711    C
712    C
713    C
714    C
715    C
716    C
717    C
718    C
719    C
720    C
721    C
722    C
723    C
724    C
725    C
726    C
727    C
728    C
729    C
730    C
731    C
732    C
733    C
734    C
735    C
736    C
737    C
738    C
739    C
740    C
741    C
742    C
743    C
744    C
745    C
746    C
747    C
748    C
749    C
750    C
751    C
752    C
753    C
754    C
755    C
756    C
757    C
758    C
759    C
760    C
761    C
762    C
763    C
764    C
765    C
766    C
767    C
768    C
769    C
770    C
771    C
772    C
773    C
774    C
775    C
776    C
777    C
778    C
779    C
780    C
781    C
782    C
783    C
784    C
785    C
786    C
787    C
788    C
789    C
790    C
791    C
792    C
793    C
794    C
795    C
796    C
797    C
798    C
799    C
800    C
801    C
802    C
803    C
804    C
805    C
806    C
807    C
808    C
809    C
810    C
811    C
812    C
813    C
814    C
815    C
816    C
817    C
818    C
819    C
820    C
821    C
822    C
823    C
824    C
825    C
826    C
827    C
828    C
829    C
830    C
831    C
832    C
833    C
834    C
835    C
836    C
837    C
838    C
839    C
840    C
841    C
842    C
843    C
844    C
845    C
846    C
847    C
848    C
849    C
850    C
851    C
852    C
853    C
854    C
855    C
856    C
857    C
858    C
859    C
860    C
861    C
862    C
863    C
864    C
865    C
866    C
867    C
868    C
869    C
870    C
871    C
872    C
873    C
874    C
875    C
876    C
877    C
878    C
879    C
880    C
881    C
882    C
883    C
884    C
885    C
886    C
887    C
888    C
889    C
890    C
891    C
892    C
893    C
894    C
895    C
896    C
897    C
898    C
899    C
900    C
901    C
902    C
903    C
904    C
905    C
906    C
907    C
908    C
909    C
910    C
911    C
912    C
913    C
914    C
915    C
916    C
917    C
918    C
919    C
920    C
921    C
922    C
923    C
924    C
925    C
926    C
927    C
928    C
929    C
930    C
931    C
932    C
933    C
934    C
935    C
936    C
937    C
938    C
939    C
940    C
941    C
942    C
943    C
944    C
945    C
946    C
947    C
948    C
949    C
950    C
951    C
952    C
953    C
954    C
955    C
956    C
957    C
958    C
959    C
960    C
961    C
962    C
963    C
964    C
965    C
966    C
967    C
968    C
969    C
970    C
971    C
972    C
973    C
974    C
975    C
976    C
977    C
978    C
979    C
980    C
981    C
982    C
983    C
984    C
985    C
986    C
987    C
988    C
989    C
990    C
991    C
992    C
993    C
994    C
995    C
996    C
997    C
998    C
999    C
1000   C

```

SUBROUTINE LETTER		74/74	OPT=1	FTN 4.8-518	10/06/80	09.37.33
1	C					
5	C	SURROUTINE LETTER				
10	100 6001 6002	DIMENSION ITITLE(12) WRITE(6*6001) DO 1000 L=1,4 READ(5,1001) ITITLE(I), I=1,12 FORMAT(12A1) FORMAT(1H-) CALL CHARAC(ITITLE) WRITE(6*6002) CONTINUE RETURN END				
15	1000 9000	AFRUM 897 AFRUM 898 AFRUM 899 AFRUM 900 AFRUM 901 AFRUM 902 AFRUM 903 AFRUM 904 AFRUM 905 AFRUM 906 AFRUM 907 AFRUM 908 AFRUM 909 AFRUM 910 AFRUM 911 AFRUM 912 AFRUM 913 AFRUM 914 AFRUM 915				



10/06/80 09.37.33

FTN 4.8+518

74/74 OPT=1

```

SUBROUTINE CHARAC 74/74 OPT=1
C
C
C
SUBROUTINE CHARAC(ITITLE)
C
C
C
DIMENSION ICHAR(37,12),IALPHA(37),ID(12),ITITLE(12),MASK(11),
LINE(135),
INTEGER OFFSET
DATA ICHAR(01,K) K=1,12 /
.01608,03708,06148,14068,14068,17768,17768,14068,14068,
.14068,14068,
DATA ICHAR(2,K) K=1,12 /
.17708,17748,14068,14068,14068,17748,17748,14068,14068,
.17748,17708,
DATA ICHAR(3,K) K=1,12 /
.03768,07768,16008,14008,14008,14008,14008,14008,16008,
.07768,03768,
DATA ICHAR(4,K) K=1,12 /
.17708,17748,14168,14068,14068,14068,14068,14068,14168,
.17748,17708,
DATA ICHAR(5,K) K=1,12 /
.017768,017768,017768,017768,017768,017768,017768,017768,
.017768,017768,017768,017768,
DATA ICHAR(6,K) K=1,12 /
.01768,01768,01768,01768,01768,01768,01768,01768,
.01768,01768,01768,01768,
DATA ICHAR(7,K) K=1,12 /
.14068,14148,14308,14608,15408,15408,14608,14308,14148,
.14068,
DATA ICHAR(8,K) K=1,12 /
.10*14008,2*17768,
DATA ICHAR(9,K) K=1,12 /
.14068,16168,17368,2*15668,14468,6*14068,
DATA ICHAR(10,K) K=1,12 /
.14068,14068,16068,17068,2*15468,2*14668,14368,14168,14068,14068,
DATA ICHAR(11,K) K=1,12 /
.03708,07748,8*14068,07748,03708,
DATA ICHAR(12,K) K=1,12 /
.17708,17748,2*14068,17748,17708,6*14008,
DATA ICHAR(13,K) K=1,12 /
.03708,07748,6*14068,14668,14368,07748,03708,
DATA ICHAR(14,K) K=1,12 /
.17708,17748,2*14068,17748,17708,15408,14608,14308,14148,2*14068,
DATA ICHAR(15,K) K=1,12 /
.03768,07768,3*14008,07708,03748,3*00068,17748,17708,
DATA ICHAR(16,K) K=1,12 /
.2*17768,10*1608,
DATA ICHAR(17,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(18,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(19,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(20,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(21,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(22,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(23,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(24,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(25,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(26,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(27,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(28,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(29,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(30,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(31,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(32,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(33,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(34,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(35,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(36,K) K=1,12 /
.017408,07728,03708,
DATA ICHAR(37,K) K=1,12 /
.017408,07728,03708,

```

```

65      3*1406B,2*0614B,0330B,6*0160B/
      DATA(CHAR(26,K),K=1,12)/
      2*1776B,0006B,0014B,0030B,0060B,0140B,0300B,0600B,1400B,2*1776B/
      DATA(CHAR(27,K),K=1,12)/
      12*0/
      DATA(CHAR(29,K),K=1,12)/
      2*1776B,8*1406B,2*1776B/
      DATA(CHAR(29,K),K=1,12)/
      0060B,0160B,0360B,7*0060B,2*0776B/
      DATA(CHAR(30,K),K=1,12)/
      2*1776B,3*0014B,0030B,0060B,0140B,0300B,0600B,2*1776B/
      DATA(CHAR(31,K),K=1,12)/
      2*1776B,3*0006B,2*0376B,3*0006B,2*1776B/
      DATA(CHAR(32,K),K=1,12)/
      0016B,0036B,0066B,0146B,0306B,0776B,1776B,5*0006B/
      DATA(CHAR(33,K),K=1,12)/
      2*1776B,2*1400B,2*1776B,4*0006B,2*1776B/
      DATA(CHAR(34,K),K=1,12)/
      2*1776B,3*1400B,2*1776B,3*1406B,2*1776B/
      DATA(CHAR(35,K),K=1,12)/
      2*1776B,2*0006B,0014B,2*0030B,5*0060B/
      DATA(CHAR(36,K),K=1,12)/
      2*1776B,3*1406B,2*1776B,3*1406B,2*1776B/
      DATA(CHAR(37,K),K=1,12)/
      2*1776B,3*1406B,2*1776B,3*0006B,2*1776B/
      DATA(CHAR(38,K),K=1,12)/
      1HM,1H0,1HP,1HQ,1HR,1HS,1HT,1HU,1HV,1HW,1HX,1HY,1HZ,1H,1H0,1H1,
      1H2,1H3,1H4,1H5,1H6,1H7,1H8,1H9/
      DATA LINE1(135,1H/
      DATA MASK/2000B,1000B,400B,200B,100B,40B,20B,10B,4B,2B,1B/
      DO 150 IJ=1,12
      J=13-IJ
      IF (TITLE(J).NE.ALPHA(27)) GO TO 70
      150 CONTINUE
      70 CONTINUE
      NUMLET=J
      OFFSET=(12-NUMLET)*6
      ITEST=0
      IJ=1
      DO 250 IJ=1,12
      JK=1
      IF (ALPHA(IJ).EQ.ALPHA(JK)) ITEST=1
      IF (ITEST.NE.0) GO TO 251
      GO TO 250
      251 CONTINUE
      250 CONTINUE
      DO 2000 LNCNT=1,12
      LPOS=1
      IPOS=(1+(LPOS-1))*OFFSET
      DO 1200 MAKEUP=1,11
      LTEST=CHAR(IPOS,LPOS,LNCNT).AND.MASK(MAKEUP)
      IF (LTEST.EQ.0) GO TO 1200
      LINE1(IPOS,MAKEUP)=IHO
      1200 CONTINUE
      1000 CONTINUE
      WRITE(6,200)(LINE1(IJ),IJ=1,135)
      DO 600 IK=1,135
      IF (LINE1(IK).EQ.IHO) LINE1(IK)=IMX
      WRITE(6,201)(LINE1(IJ),IJ=1,135)
      DO 601 IK=1,135
      IF (LINE1(IK).EQ.IMX) LINE1(IK)=IMA
      WRITE(6,201)(LINE1(IJ),IJ=1,135)
      DO 602 IK=1,135
      IF (LINE1(IK).EQ.IMA) LINE1(IK)=IMV
      WRITE(6,201)(LINE1(IJ),IJ=1,135)
      201 FORMAT(1H,135A1)
      DO 106 IJ=1,135
      LINE1(IJ)=IH
      106 CONTINUE
      2000 CONTINUE
      RETURN
      END

```

```

AFRUM 980
AFRUM 981
AFRUM 982
AFRUM 983
AFRUM 984
AFRUM 985
AFRUM 986
AFRUM 987
AFRUM 988
AFRUM 989
AFRUM 990
AFRUM 991
AFRUM 992
AFRUM 993
AFRUM 994
AFRUM 995
AFRUM 996
AFRUM 997
AFRUM 998
AFRUM 999
AFRUM 1000
AFRUM 1001
AFRUM 1002
AFRUM 1003
AFRUM 1004
AFRUM 1005
AFRUM 1006
AFRUM 1007
AFRUM 1008
AFRUM 1009
AFRUM 1010
AFRUM 1011
AFRUM 1012
AFRUM 1013
AFRUM 1014
AFRUM 1015
AFRUM 1016
AFRUM 1017
AFRUM 1018
AFRUM 1019
AFRUM 1020
AFRUM 1021
AFRUM 1022
AFRUM 1023
AFRUM 1024
AFRUM 1025
AFRUM 1026
AFRUM 1027
AFRUM 1028
AFRUM 1029
AFRUM 1030
AFRUM 1031
AFRUM 1032
AFRUM 1033
AFRUM 1034
AFRUM 1035
AFRUM 1036
AFRUM 1037
AFRUM 1038
AFRUM 1039
AFRUM 1040
AFRUM 1041
AFRUM 1042
AFRUM 1043
AFRUM 1044
AFRUM 1045
AFRUM 1046
AFRUM 1047
AFRUM 1048
AFRUM 1049
AFRUM 1050
AFRUM 1051
AFRUM 1052
AFRUM 1053

```

# INITIAL DISTRIBUTION

OUSDR&E	1
OSAF/MIQ	1
DTIC/DDA	2
OSAF/PA	1
HQ USAF/LEEV	1
OEHL/CC	2
USAFSAM/EDH	1
USAFSAM/VNL	1
USAF Hospital Wiesbaden/SGB	1
AUL/LSE 71-249	1
HQ USAFA/Library	1
AFRPL/Library	1
AFATL/DLODL	1
Ch, Pollution Abatement Br	
NAVFAC Code 111	1
NESO	1
NCEL, Code 15111	1
HQ AFESC/TST	1
HQ AFESC/RDVA	10
AFIT/Library	1
102 ABG/DEEV	1
University of Tennessee	3
HQ 305 CSG/DEEV-1	1
EPA/R&D	1
Overton & Associates, Inc.	1
USAFRCE/WR/DEEV	1
USAFRCE/CR/DEEV	1
USAFRCE/ER/DEEV	1

**DATE**  
**FILME**